

THE DESIGN OF A DOUBLE-POINT CALIBRATION ROUTINE
FOR A MULTICHANNEL HYPERTHERMIA THERMOMETRY SYSTEM

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THESIS

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CHAPTER I

INTRODUCTION

Hyperthermia is the use of elevated temperatures to treat cancerous tumors. The selective heating of the unhealthy tissue alters the state of the abnormal cells allowing the radiation treatment which follows to be more effective.

A block diagram of a hyperthermia system is shown in Figure 1.1. The thermometry unit is a critical part of this system. The temperature of the tumor and the normal tissue surrounding it must be monitored at several locations. For the best results, the temperature of the abnormal tissue is kept above the minimum treatment level of about 43°C , but below an upper tolerance level of approximately 50°C . In addition, the encircling healthy tissue is maintained below 40°C , as near to normal tissue temperature as possible. The temperature information obtained is used to determine the level of ultrasound or microwave energy the controller sends to the tissue via the applicator.

The thermometry system may also function as a stand-alone unit. As indicated by the dashed line in Figure 1.1, the thermometry unit may connect directly to a terminal, via an RS-232 connection, for the input and output interactions with an operator.

Since the thermometry hardware has varying gain and offset characteristics for each channel, a calibration of the system is required before treatment may begin. The double-point calibration scheme will be discussed and analyzed in this thesis.

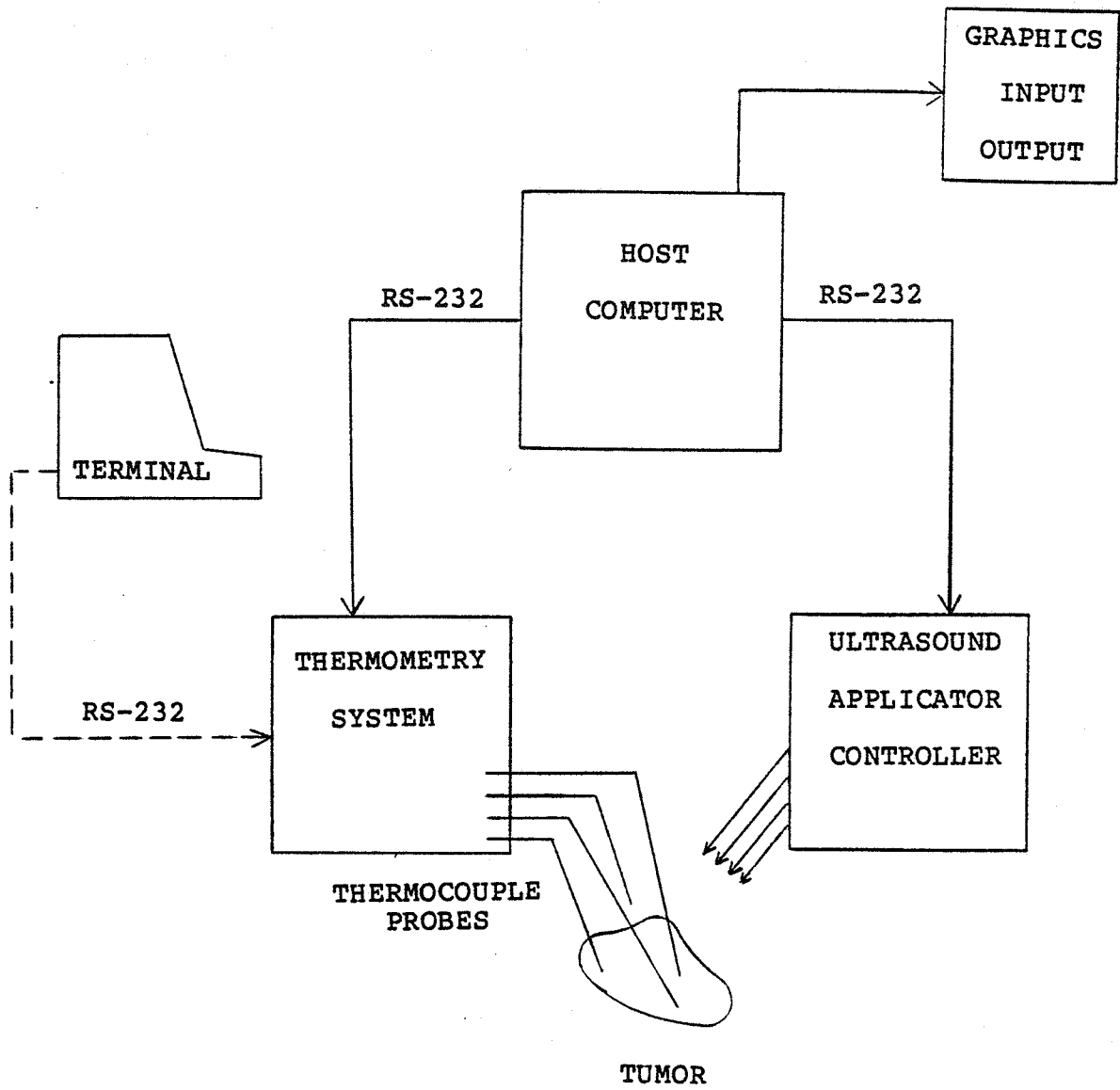


Figure 1.1. Block diagram of a hyperthermia system.

CHAPTER II

THERMOMETRY HARDWARE OVERVIEW

The thermometry system is based on the Intel 8031 microcontroller as designed by Alfred Gharakhani [1]. A block diagram of the system is displayed in Figure 2.1. The temperatures are obtained through the use of type T (copper-constantan) thermocouple probes. The probes generate voltages based on the temperature at the copper-constantan junctions. Then, the voltages are amplified and one channel is selected by the analog multiplexer. At this time, the error detection circuitry signals the 8031 if the probe for the channel chosen is broken or missing. Otherwise, the voltage from the analog multiplexer is scaled so that the analog-to-digital (A/D) converter functions correctly. The twelve bits of digitized voltage are sent to the 8031 for further software processing. The temperature corresponding to the particular voltage is transmitted to the terminal via the RS-232 connection in appropriate ASCII code.

The conversion between thermocouple voltage and temperature requires either a look-up table or an equation which models the table. Complications encountered in the look-up table method necessitated the use of a polynomial equation to model the conversion. In addition, each channel of hardware may have a different gain and offset which requires a linear fit. These two situations are dealt with by calibrating the thermometry system to a precision thermometer before any readings are made.

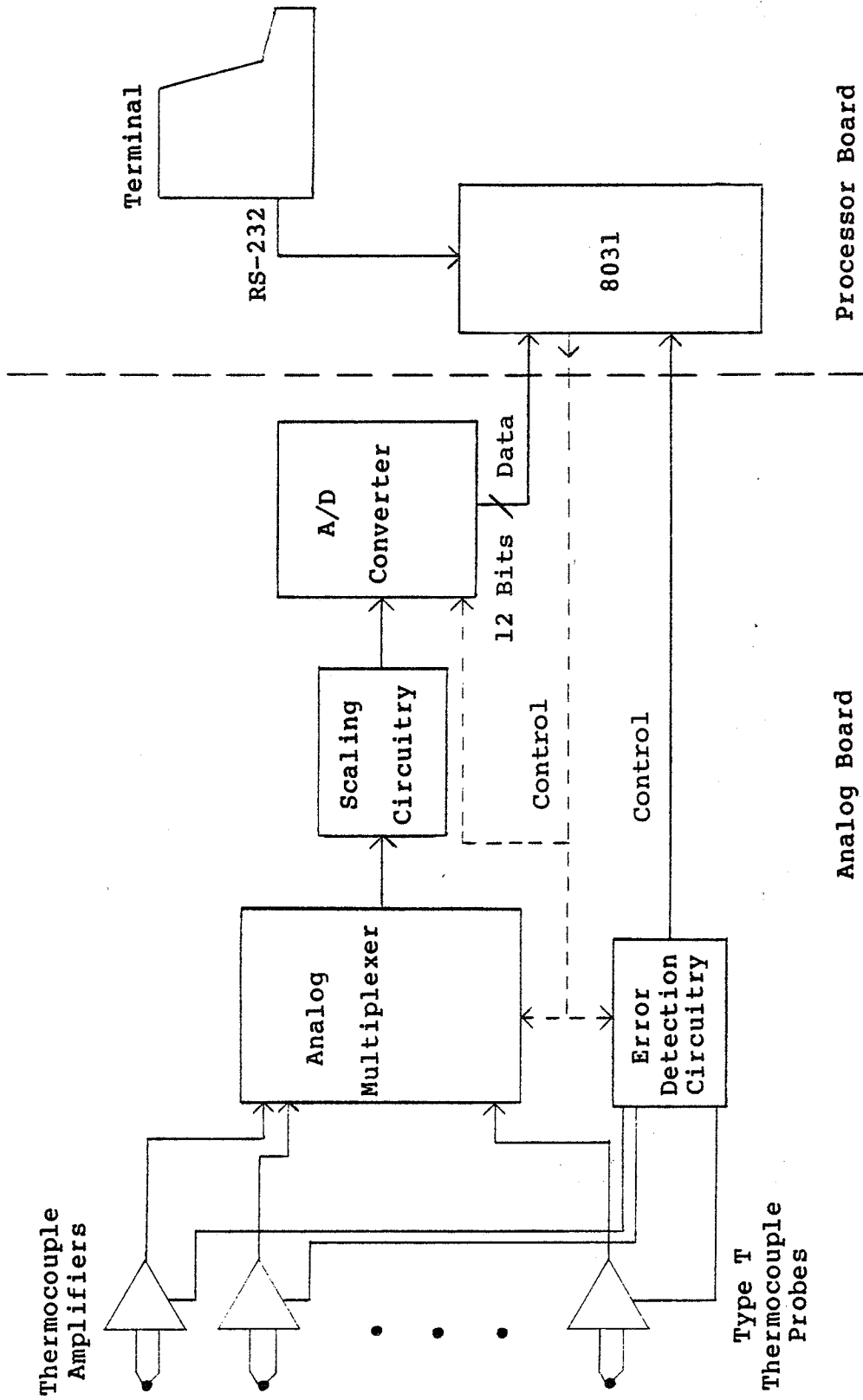


Figure 2.1. Block diagram of the thermometry unit (from [1]).

To improve the thermometry system and its calibration, several changes have been made to Gharakhani's design. A summary of the major modifications is described below.

The type J (iron-constantan) thermocouple probes and the corresponding thermocouple amplifier chips, which Gharakhani used, were replaced by type T (copper-constantan) thermocouple probes and amplifiers. The type T probes are more resistant to corrosion in moist surroundings [2], whereas the type J probes will rust if placed in a water bath for an extended length of time.

The valid temperature range of 0°C to 51.1°C was changed to 20°C to 60°C , and the least significant digit changed from 0.1°C to 0.01°C . It will turn out that the calibration calculations work for temperatures in the range 0°C to 99.99°C , but the thermocouple voltage to temperature conversion is accurate only for the range 20°C to 60°C .

Since the temperature output is to the hundredth place, the look-up table scheme for the conversion between thermocouple voltage and temperature could no longer be used. For the range 0°C to 51.1°C , the look-up table consisted of 512 memory locations for each of the three numeric places (stored as ASCII characters). That is equivalent to 1,536 locations. For output temperatures to the hundredth place, in the range 20°C to 60°C , the look-up table scheme would require $4001 * 4 = 16,004$ bytes, a considerable amount of memory. Moreover, if the temperature was out of the range of values in the look-up table, an underflow or overflow error would occur. The extended range of 0°C to 99.99°C would require $10,000 * 4 = 40,000$ memory locations. Obviously, it would be wasteful to attempt this method. Fortunately, the look-up

table may be replaced by a polynomial equation approximating the conversion. This scheme will be discussed further in Chapter III.

Another significant change is that all twelve bits of data from the analog-to-digital converter are used rather than only nine bits. This will increase the accuracy of the displayed temperatures.

Furthermore, the two calibration points are user selectable rather than set at 25°C and 35°C.

These changes will result in a more accurate and "user-friendly" system.

CHAPTER III

THERMOCOUPLE CHARACTERISTICS

3.1. Nonlinearity

Thermocouples have many characteristics advantageous for ultrasound hyperthermia temperature measurement. They are sturdy, small in size, and respond quickly; however, the thermocouple output voltage is nonlinear with respect to temperature [3]. A plot of the type T thermocouple voltage versus temperature, for the range 20°C to 60°C, is shown in Figure 3.1. This is a graphical representation of the thermocouple reference table from [4], which is reproduced in Table 3.1.

As can be seen, the nonlinearity does not appear to be severe. Nevertheless, further calculations will indicate the advantage of taking the nonlinearity into account. Note also that the design will actually have one hundred points between the ones shown in Figure 3.1, since the resolution is to 0.01°C.

For the double-point calibration and correction of the thermometry system, four main equations are required. Two of these are the nonlinear conversions between thermocouple voltage and temperature. The other two involve a simple linear model of the system hardware. The thermocouple conversion equations are based on the type T standard reference table displayed in Table 3.1. These equations will be discussed in the following two subsections. The other equations and the calibration scheme itself will be presented in Chapter IV.

3.1.1. Conversion of Thermocouple Voltage to Temperature

The conversion from thermocouple voltage to temperature, for

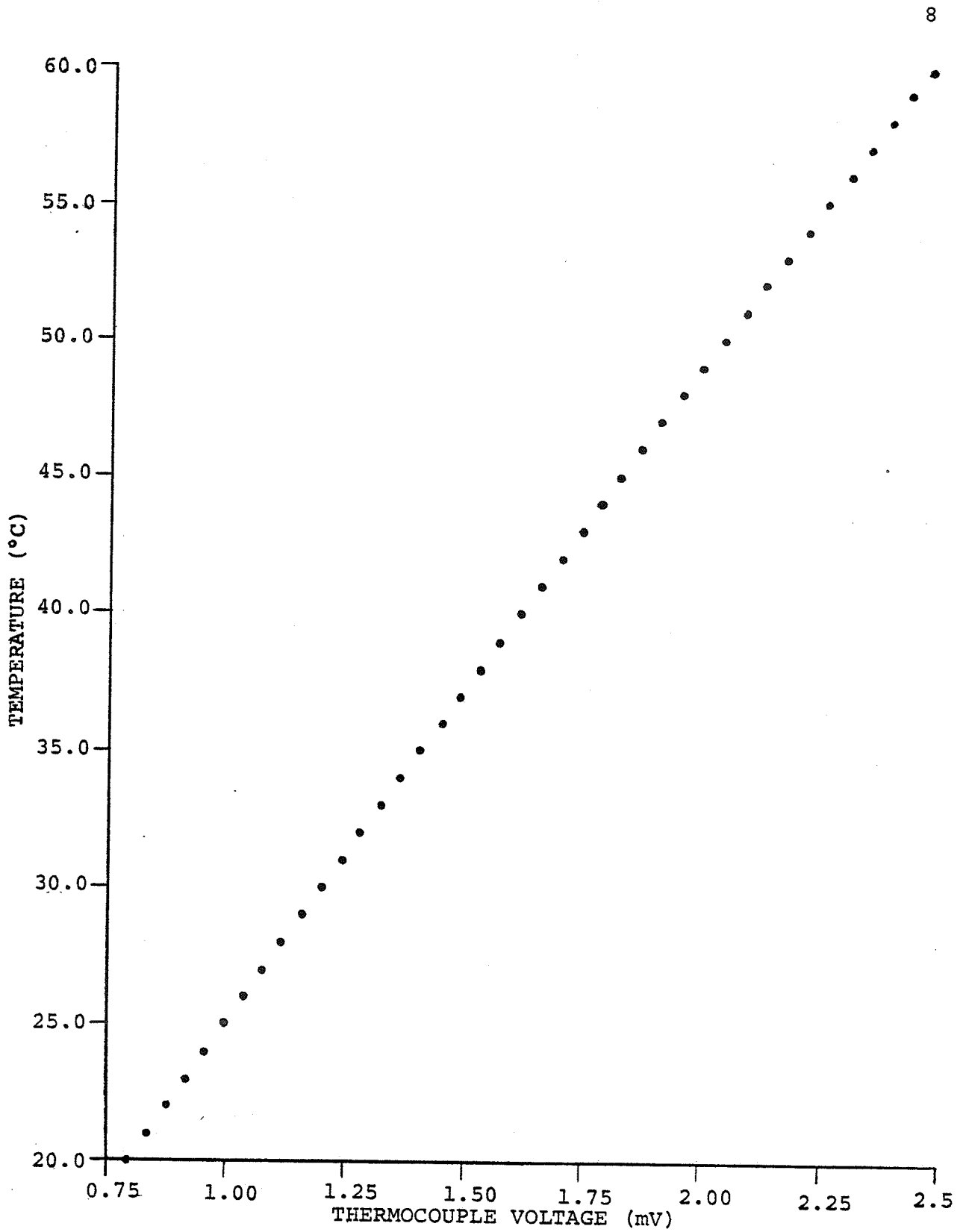


Figure 3.1. Temperature - voltage correspondence for type T thermocouples.

Table 3.1. Temperature - Voltage Correspondence
for Type T Thermocouples (from [4]).

<u>Temperature (°C)</u>	<u>Voltage (mV)</u>	<u>Temperature (°C)</u>	<u>Voltage (mV)</u>
20	0.789	40	1.611
21	0.830	41	1.653
22	0.870	42	1.695
23	0.911	43	1.738
24	0.951	44	1.780
25	0.992	45	1.822
26	1.032	46	1.865
27	1.073	47	1.907
28	1.114	48	1.950
29	1.155	49	1.992
30	1.196	50	2.035
31	1.237	51	2.078
32	1.279	52	2.121
33	1.320	53	2.164
34	1.361	54	2.207
35	1.403	55	2.250
36	1.444	56	2.294
37	1.486	57	2.337
38	1.528	58	2.380
39	1.569	59	2.424
40	1.611	60	2.467

20°C to 60°C, was calculated using a best polynomial fit. The resulting equations are of the form

$$T = A3 * V^3 + A2 * V^2 + A1 * V + A0 \quad (3.1)$$

where A3, A2, A1, and A0 are real constants, which may be zero, T is temperature in degrees Celsius, and V is voltage in millivolts. The constants are shown in Table 3.2 for zero order, linear, quadratic, and cubic fits. The zero order equation is obviously not a good fit, but it is included for the purpose of comparison.

Also shown in Table 3.2 are the mean square error (or variance) and the root mean square (RMS) error (or standard deviation) as defined by

$$\text{Mean Square} = [\Sigma(T - T_i)^2] / N \quad (3.2)$$

and

$$\text{RMS} = [[\Sigma(T - T_i)^2] / N]^{1/2} \quad (3.3)$$

The value of T_i is the ideal temperature from Table 3.1, and its corresponding voltage is V. T is the temperature calculated from Equation (3.1), using the value of voltage, V, and the appropriate values of the constants, for each particular fit in Table 3.2. N is the number of data points, a total of forty-one, in Table 3.1.

To determine which equation to use, the RMS error values were compared. As the order of the equation increases, the RMS error decreases. Notice that there is an improvement of 0.1197°C in the RMS error between the linear and quadratic equations. However, there is only a difference of 0.0007°C in the RMS error between the quadratic and cubic approximations. In other words, the RMS error accompanying the second and third order fits is smaller than

Table 3.2. Polynomial Fits for the Conversion from Thermocouple Voltage to Temperature.

	ZERO	ORDER OF FIT		
		LINEAR	QUADRATIC	CUBIC
A3	0	0	0	0.0329830244
A2	0	0	-0.577516124	-0.7384273168
A1	0	23.8349418	25.7112919	25.95831205
A0	40	1.45134171	0.0696651191	-0.048435657
MEAN SQUARE (°C) ²	140	0.0162	0.000057891	0.000048047
RMS (°C)	11.8322	0.1274	0.0076	0.0069
MAXIMUM DEVIATION (°C)	+20	+0.2571	-0.0154	+0.0133

the desired resolution of 0.01°C .

The values in Table 3.1 have finite precision and, thus, an inherent round-off error. The precision in the voltage values is $1\ \mu\text{V}$ and the theoretical round-off error [5] is

$$1\ \mu\text{V} / [(12^{1/2})] = 0.289\ \mu\text{V}. \quad (3.4)$$

This corresponds to

$$0.289\ \mu\text{V} / (40.44\ \mu\text{V}/^{\circ}\text{C}) = 0.0071^{\circ}\text{C} \quad (3.5)$$

where $40.44\ \mu\text{V}/^{\circ}\text{C}$ is the input offset voltage per degree of temperature change (from [3]). This value of 0.0071°C is the theoretical value of the RMS error, and it indicates the smallest error that can be statistically realized. As seen in Table 3.2, the higher order fits approach this value and, in fact, the cubic fit has an RMS error that is smaller than 0.0071°C . This is misleading, though, since as N approaches infinity, the RMS error has to approach 0.0071°C .

Another factor to consider is the maximum deviation, also shown in Table 3.2. The calculated and ideal temperatures were compared for every degree between 20°C and 60°C . Again, the magnitudes of the deviation for the quadratic and cubic fits are close in value.

There are trade-offs in choosing which equation is the best to use for this application. The cubic equation has slightly smaller errors, but the extra calculations and several special routines required were not considered to be worth the small gain in accuracy. The equation is then

$$T = -0.577516124 * V^2 + 25.7112919 * V + 0.0696651191 \quad (3.6)$$

where T is the temperature in degrees Celsius and V is the voltage in millivolts.

3.1.2. Conversion of Temperature to Thermocouple Voltage

The best polynomial fit for the conversion from temperature to thermocouple voltage is of the form

$$V = B3 * T^3 + B2 * T^2 + B1 * B0 \quad (3.7)$$

where B3, B2, B1, and B0 are real constants, V is voltage in millivolts, and T is temperature in degrees Celsius. The constants are shown in Table 3.3 for zero order, linear, quadratic, and cubic fits. Also displayed are the mean square error, RMS error, and maximum deviation.

The round-off error due to the finite precision of Table 3.1 is 0.289 μ V, as stated in Equation (3.4). For this conversion, the RMS errors for the quadratic and cubic fits are exactly equal. In addition, the quadratic fit has a smaller maximum deviation for the points examined. For these reasons, the quadratic fit has been chosen again. This equation is

$$V = 0.0000426489542 * T^2 + 0.0385384869 * T + 0.00157115981 \quad (3.8)$$

where V is voltage in millivolts and T is temperature in degrees Celsius.

Equations (3.6) and (3.8) are shown with constants that have several significant digits. Naturally, when these equations are implemented on the eight bit Intel 8031 microcontroller, some of the accuracy will be lost. A further discussion on this matter appears in Chapter IV.

Table 3.3. Polynomial Fits for the Conversion from Temperature to Thermocouple Voltage.

	ZERO	ORDER OF FIT		
		LINEAR	QUADRATIC	CUBIC
B3	0	0	0	6.190*10 ⁻¹³
B2	0	0	0.0000426489542	4.2606*10 ⁻⁵
B1	0	0.0419503489	0.0385384869	0.038541969
B0	1.611	-0.0606968815	0.00157115981	0.001502803
MEAN SQUARE (μV) ²	243.8693	28.5543	0.0848	0.0848
RMS (μV)	493.8312	5.3436	0.2912	0.2912
MAXIMUM DEVIATION (μV)	+856	-10.6899	-0.5265	-0.5334

3.2. Self-Heating Effects

The tip of the type T thermocouple is a junction of two metals, copper and constantan. At the point of contact, a potential difference exists which is a repeatable function of temperature [3]. In order to relate this voltage to temperature, a known reference temperature is necessary.

Usually, standard thermocouple voltage to temperature conversion tables assume a reference junction at 0°C. The thermocouple amplifier used in the thermometry system, the AD595, has an effective reference junction which is not at 0°C. This junction is shown in Figure 3.2 at point A. Here, a second thermocouple junction exists which must be kept at the same temperature as the AD595. If the temperature is maintained, the cold junction compensation feature of the AD595 will work properly. Internally, the compensation voltage (V_0 in Figure 3.2) adds to the thermocouple voltage an amount proportional to the difference between 0°C and the AD595 temperature. Thus, the output voltage will be equivalent to a reading from a thermocouple referenced to an ice bath [3].

This design seems to account for the self-heating effects of the thermocouple amplifier chip; however, there is a problem. The specification for the AD595 [3] indicates that the input offset change with respect to temperature is typically

$$dV_0/dT = 40.44 \mu V/^{\circ}C \quad (3.9)$$

at 25°C. This implies that, ideally, the change in thermocouple voltage with respect to temperature should also be 40.44 $\mu V/^{\circ}C$ for the compensation to function correctly. The change in

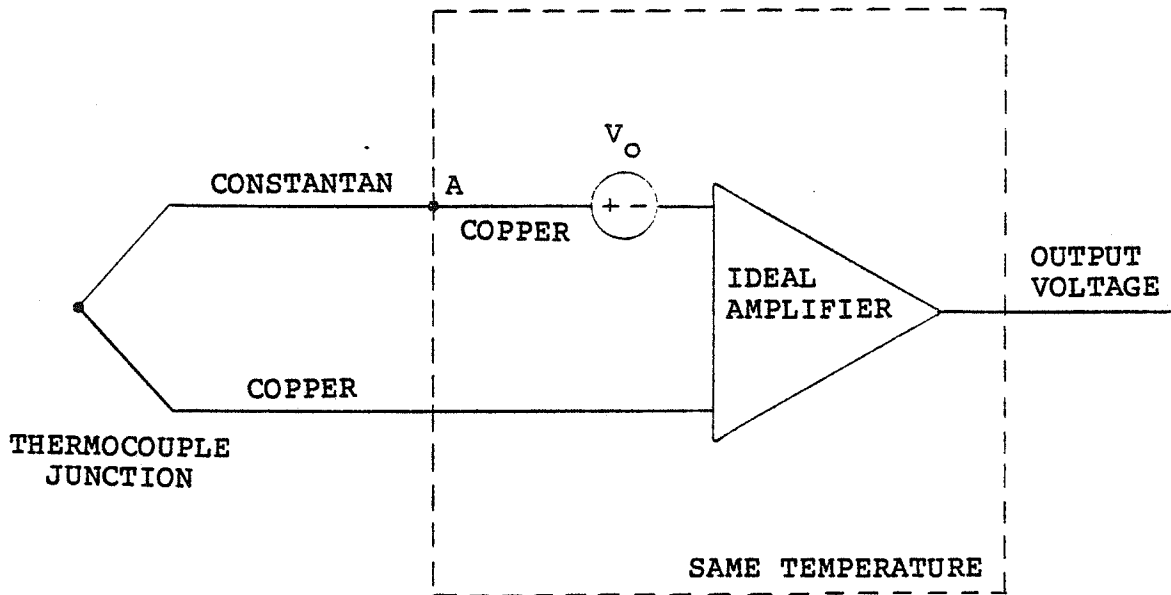


Figure 3.2. Thermocouple amplifier showing the effective reference junction at A.

thermocouple voltage with respect to temperature may be calculated by finding the derivative of Equation (3.8). That is

$$dV_{th}/dT = 0.0852979084 * T + 38.5384869 \text{ } \mu\text{V}/^{\circ}\text{C}. \quad (3.10)$$

Table 3.4 shows the voltage change as the ambient temperature increases. Here, compensation and deviation are defined as

$$\text{Compensation} = dV_{th}/dT - 40.44 \text{ } \mu\text{V}/^{\circ}\text{C} \quad (3.11)$$

and

$$\text{Deviation} = (dV_{th}/dT - 40.44) / (dV_{th}/dT). \quad (3.12)$$

Table 3.4. Ambient Temperature Effects.

Ambient Temperature ($^{\circ}\text{C}$)	dV_{th}/dT ($\mu\text{V}/^{\circ}\text{C}$)	Compensation ($\mu\text{V}/^{\circ}\text{C}$)	Deviation ($\frac{^{\circ}\text{C}}{^{\circ}\text{C}}$)
20	40.24	-0.20	-0.005
22.3	40.44	0.00	0.000
25	40.67	+0.23	+0.006
30	41.1	+0.66	+0.016
35	41.52	+1.08	+0.026
40	41.95	+1.51	+0.036

The cold junction compensation of the AD595 compensates incorrectly for ambient temperatures other than 22.3 $^{\circ}\text{C}$. Obviously, if the chip temperature is allowed to increase much above 25 $^{\circ}\text{C}$, some error will result. Notice that the dV_o/dT and dV_{th}/dT do not match at 25 $^{\circ}\text{C}$. This is because the AD595 is intended to operate with type K thermocouples (the copper is replaced by a nickel-chromium alloy in the ratio 90:10) and produce zero compensation at 25 $^{\circ}\text{C}$.

Another specification of the AD595, related to self-heating effects, is the stability versus temperature. This value is rated at $\pm 0.025^{\circ}\text{C}/^{\circ}\text{C}$ [3]. Since type T rather than type K thermocouples are being used, the $+0.006^{\circ}\text{C}/^{\circ}\text{C}$ deviation, taken from Table 3.4, should be added to the $\pm 0.025^{\circ}\text{C}/^{\circ}\text{C}$ rating at 25°C . For example, suppose a reading of 37°C were obtained when the ambient temperature was 25°C . Then, if the ambient temperature increases by one degree to 26°C , the uncertainty in the reading will be -0.02°C to $+0.03^{\circ}\text{C}$. This implies that the reading may be between 36.98°C and 37.03°C just due to the increase in ambient temperature by one degree.

At other ambient temperatures, the results get worse. For instance, at 30°C , the error is $\pm 0.025^{\circ}\text{C}/^{\circ}\text{C}$, plus the value $+0.016^{\circ}\text{C}/^{\circ}\text{C}$ from Table 3.4. Thus, the uncertainty is -0.01°C to $+0.04^{\circ}\text{C}$, and the reading may be between 36.99°C and 37.04°C , just because of the ambient temperature change.

From this discussion, it is apparent that some means of controlling the ambient AD595 temperature is advisable.

CHAPTER IV
THE CALIBRATION SCHEME

4.1. Description and Procedure

Since each channel of the thermometry system has different thermocouple amplifier chips with slightly different characteristics, each probe, if uncalibrated, may output a different temperature. The purpose of the calibration program is to correct hardware deviations.

From the user's point of view, the double-point calibration of the thermometry system is a quick and easy process. The steps are:

1. Place the probes to be used in a water bath (or oven) of constant temperature, T_1 .
2. Enter temperature T_1 on the terminal.
3. Place the probes in a bath of constant temperature, T_2 , of greater value than T_1 .
4. Enter temperature T_2 on the terminal.

Temperatures T_1 and T_2 may take on any value in the range from 20°C to 60°C . Note that the calculations in the program work for temperatures between 0°C and 99.99°C , but the nonlinear conversion equations were based on temperatures in the range 20°C to 60°C . The speed of the calibration process is limited only by the input and output interactions and the time it takes for the water bath (or oven) to stabilize at T_1 and T_2 . After the four steps, the system is calibrated. From then on, every time a reading is made, the output temperature is modified to the correct value before being displayed.

An overview of the calibration and correction process is shown in Figure 4.1. In addition, a detailed flow chart is presented in Appendix A. After the operator places the probes in temperature T1 and enters its value on the terminal, all of the probes are read. The digitized thermocouple output voltages are stored in memory. The same process of reading and storing is repeated when the probes are in temperature T2.

Next, entered temperatures T1 and T2 are converted to voltages using a form of equation (3.8). The equation actually used in the program is

$$V = 426.5 * T^2 + 38,538,486 * T + 157,115,981. \quad (4.1)$$

Here, V is in 10^{-14} volts and T is in 10^{20} C. Notice that the constants have been multiplied by 10^{11} and that some of the significant digits have been dropped. This makes calculation easier by eliminating most of the fractional parts. Actually, in the program, the value 4265 is multiplied by T^2 and then the product is divided by ten. Since all of the arithmetic operations on the Intel 8031 involve one byte long numbers, several special subroutines were written to perform multiple byte multiplication and division. In addition, some values are multiplied by factors of 256 to avoid division resulting in a fractional number. It is necessary to keep track of these adjustments so that the reverse process can be performed later to get the true values. The comments in the program listing in Appendix B explain the procedure.

The next step in the calibration, as shown in Figure 4.1, is the approximation of the system hardware by a linear fit. That

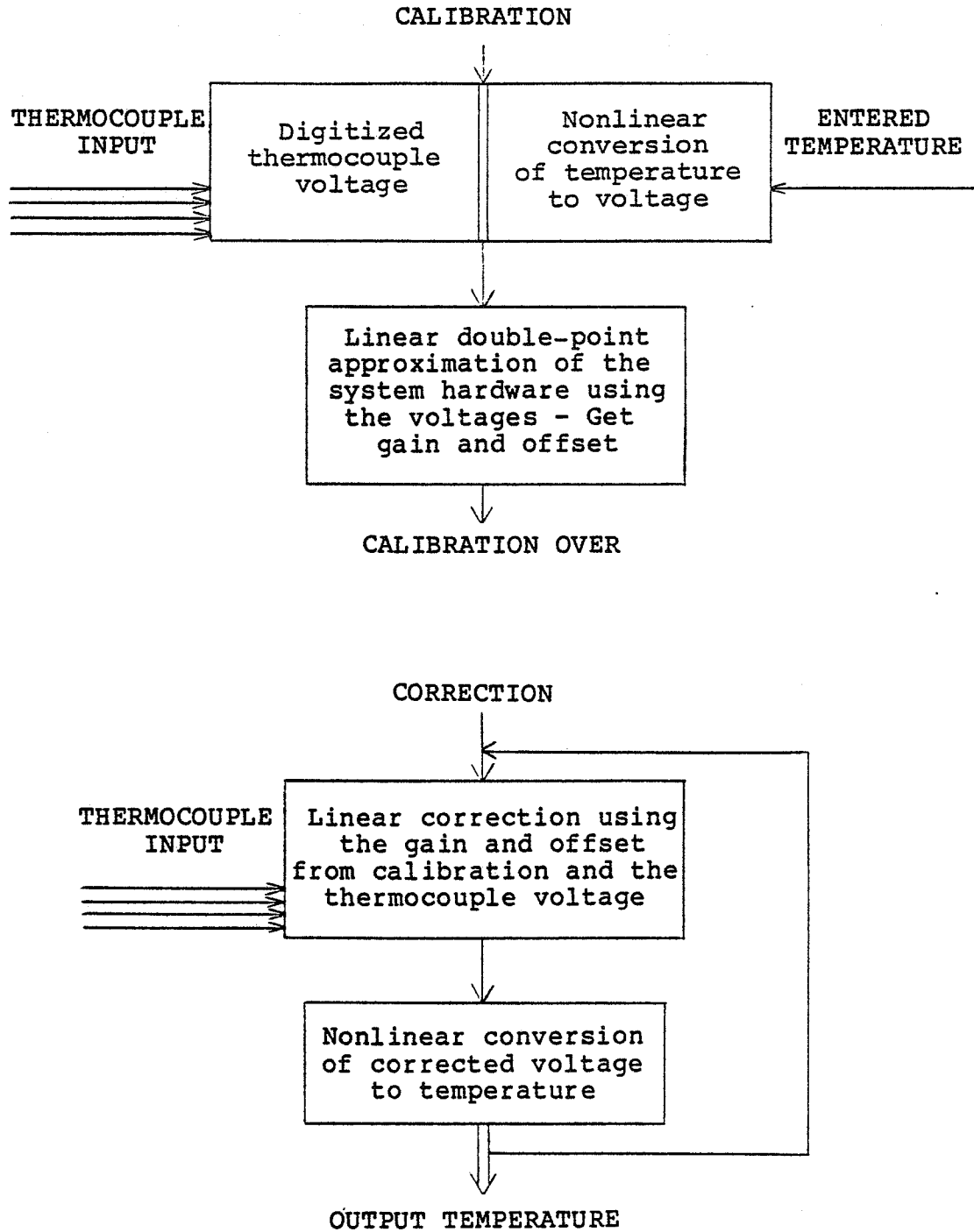


Figure 4.1. Overall calibration and correction scheme.

is, the gain and offset for each channel are found using

$$Y = M * X + B \quad (4.2)$$

where X is the known voltage obtained from the entered temperature, Y is the digitized thermocouple voltage, M is the gain, and B is the offset. Once calculated, the gain and offset for each channel are stored in memory and, at this point, the calibration is complete.

From now on, when the probes are sampled, Y, the digitized voltage obtained is corrected using the stored gain, the stored offset, and the linear equation

$$X = (Y - B) / M. \quad (4.3)$$

The corrected voltage, X, is then converted to a temperature using a form of equation (3.6). Again, due to the limitations of the microprocessor, the actual equation used is

$$T = -27.27 * V^2 + 7,237,085 * V + 116,878,675. \quad (4.4)$$

Here, T is temperature in $(100 * 256^3)$ degrees Celsius and V is voltage in $(10^{-14} * 256^3)$ volts. These units may seem odd, but the equation was put in this form to make the calculations easier.

Any of the calibrated probes may be chosen for a reading as many times as desired. However, if the probe corresponding to a particular channel was missing or broken during the calibration, then it will remain uncalibrated unless the calibration procedure is performed again. The flow chart in Appendix A shows some of the error checking present in the routine. Also, see the listing of the calibration program in Appendix B for more details [6].

4.2. An Example of Calibration

The example which follows is intended to highlight and clarify the flow chart in Appendix A. The calibration of only one probe will be considered, but the extension to any number of probes is straightforward. Notice that truncation is used in the calculations.

- Let the temperature, T_1 , of the first water bath and the twelve bit digitized voltage, Y_1 , of the probe in this water bath be:

$$T_1 = 37.06^{\circ}\text{C}$$

$$Y_1 = 05\text{DB in hexadecimal} = 1499 \text{ in decimal.}$$

- Let the temperature, T_2 , of the second water bath and the twelve bit digitized voltage, Y_2 , of the probe in this water bath be:

$$T_2 = 50.04^{\circ}\text{C}$$

$$Y_2 = 07\text{F9 in hexadecimal} = 2041 \text{ in decimal.}$$

- Temperatures ($T_1 * 100$) and ($T_2 * 100$) are converted to voltages V_1 and V_2 using equation (4.1). Then, they are each divided by 256^3 , obtaining X_1 and X_2 respectively, so that the numbers are easier to process in the 8031. However, the results are still accurate.

$$V_1 = 1.488384 * 10^{11} \qquad X_1 = 8871$$

$$V_2 = 2.036832 * 10^{11} \qquad X_2 = 12,140$$

- Next, the points (X_1, Y_1) and (X_2, Y_2) are fitted to a line using equation(4.2).

$$1499 = M * 8871 + B$$

$$2041 = M * 12,140 + B$$

- The gain, $M = m * 256^2$ is found.

$$m = (Y_2 - Y_1) / (X_2 - X_1) = 542 / 3269$$

Since (542/3269) will be a fraction, the numerator is multiplied by 256^2 , then the division is performed.

$$M = m * 256^2 = (542 * 256^2) / 3269 = 10,865$$

- The offset, $B = b * 256^2$ is found.

$$b = Y_1 - M * X_1$$

Since M is actually $(m * 256^2)$, we need $(Y_1 * 256^2)$ to get $B = (b * 256^2)$.

$$B = Y_1 * 256^2 - M * X_1 = 1,855,049.$$

- The gain and offset are stored in memory. Three bytes of memory for gain and five bytes of memory for offset are reserved for each channel.
- The calibration is over.

- The probe is placed in a water bath of temperature T. The digitized voltage, Y, of the probe is read.

$$Y = 06DB \text{ in hexadecimal} = 1755 \text{ in decimal}$$

$$T = 43.24^\circ\text{C} = \text{the desired output temperature}$$

- The correction to Y, the voltage, is made using equation (4.3) with the extra factor of 256^2 included.

$$X = (Y * 256^2 - B) / M = 10,415$$

- In this example, X is playing the role of the corrected thermocouple voltage, V. This value of voltage is used in equation (4.4) to convert to temperature, T. The result is divided by $(100 * 256^3)$ to get the actual temperature.

$$T = 7.253308 * 10^{10}$$

$$\text{Temperature} = 43.23^\circ\text{C}$$

- The temperature is transmitted to the terminal as ASCII characters for display.

The truncation of intermediate results during the calculations and the other manipulation of the values cause the final temperature to have an error of 0.01°C .

CHAPTER V
EXPERIMENTAL DATA AND ANALYSIS

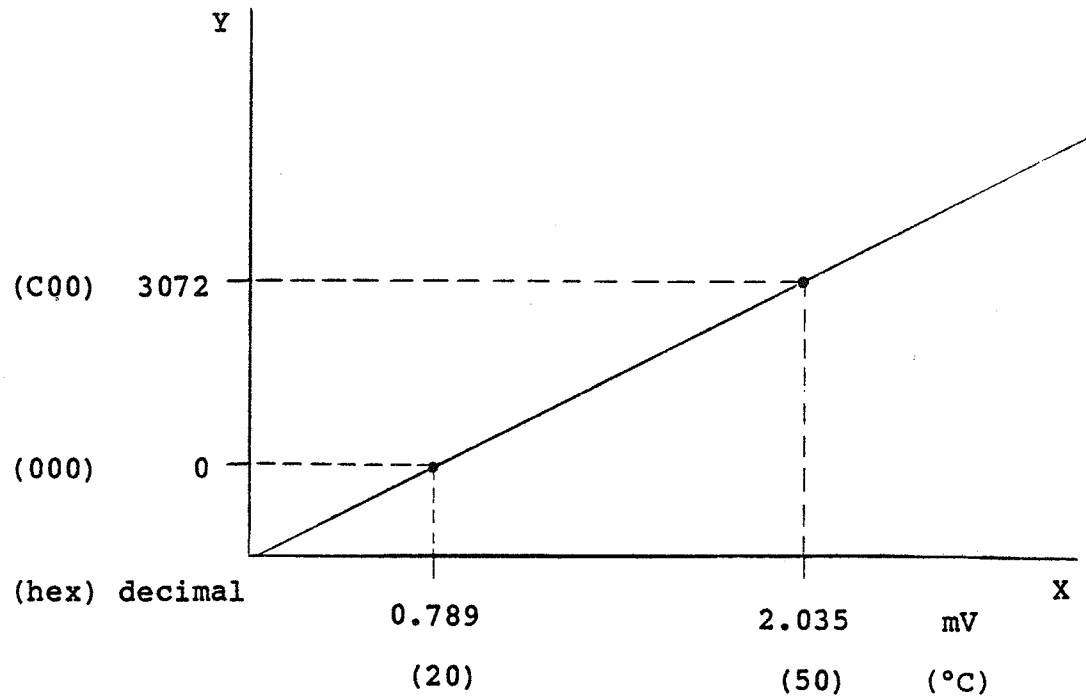
5.1. Overview

Several experimental tests of the calibration routine have been performed. These tests were designed to study the properties of accuracy, precision, stability, and repeatability. Due to hardware failure of Gharakhani's thermometry system, the input and output parts of the program were modified and the tests were performed on URI THERM-X's version of the system. It will be shown that most of the error that occurs is due to analog hardware variations. Once the calibration is complete, the correction routine will always output the same temperature when given a particular voltage.

5.2. Software Test

A test of the software was devised which eliminated the analog hardware. The calibration points were chosen to be 20°C and 50°C. Then, the twelve bit digitized voltages corresponding to these temperatures, 000 and C00 (in hexadecimal), respectively, were used instead of the usual thermocouple output voltage obtained from the analog circuitry. This means that all parts of the program were run with known numerical values.

Figure 5.1 shows the linear fit involved. On the x-axis are the temperatures, in degrees Celsius, and their equivalent voltages, in millivolts, obtained from Table 3.1. The y-axis shows the expected digitized voltage from the analog-to-digital converter corresponding to a particular temperature. The digitized voltages for various temperatures in the range 20°C to



$$M = (3072 - 0) / (2.035 - 0.789) = 2465.489$$

$$B = -1945.271$$

Figure 5.1. The linear fit of the calibration software test.

60°C were calculated by hand using the method in the calibration routine. Then, the program was executed. The results are shown in Table 5.1. The deviation displayed is the difference between the temperature obtained from the program and the ideal temperature.

There is one deviation of 0.02°C, but the rest of the time it is less. This error is directly related to the calculations in the program. As discussed in Chapter IV, the microprocessor's limitation of eight bit arithmetic operation causes unusual manipulations of intermediate values. With this in mind, the error involved is small.

In review, Table 5.1 and the discussion above indicate that an error of up to 0.02°C may be attributed to the calibration calculations in the program. Errors greater than this are hardware related.

5.3. Test Setup

All of the other tests made use of a test setup as shown in Figure 5.2. The probes were placed in a water bath of constant temperature. The accurate temperature of the water was measured using the platinum resistance thermometer (PRT). The printer gave a permanent record of the temperatures of the probes for any chosen interval of time.

An important consideration for obtaining reliable data was to make sure that the temperature of the water bath was stable, as indicated by a stable readout on the PRT. The thermocouple probes will react much quicker to a temperature change than will the PRT. Therefore, if the temperature indicated by the PRT is still changing when a reading is made, erroneous results will occur.

Table 5.1. Results of Calibration Program Check.

<u>Ideal Temperature(°C)</u>	<u>Temperature from Hand Calculation(°C)</u>	<u>Temperature from Program(°C)</u>	<u>Deviation (°C)</u>
20	20.00	20.00	0.00
23	23.00	23.01	0.01
25	25.00	25.01	0.01
28	27.99	28.00	0.00
30	29.99	29.99	0.01
33	33.00	33.00	0.00
35	34.99	35.00	0.00
38	38.00	38.01	0.01
40	39.99	39.99	0.01
43	43.00	43.01	0.01
45	44.99	44.99	0.01
48	48.00	48.01	0.01
50	50.00	50.00	0.00
52	52.00	52.00	0.00
54	53.99	54.00	0.00
58	57.98	57.98	0.02

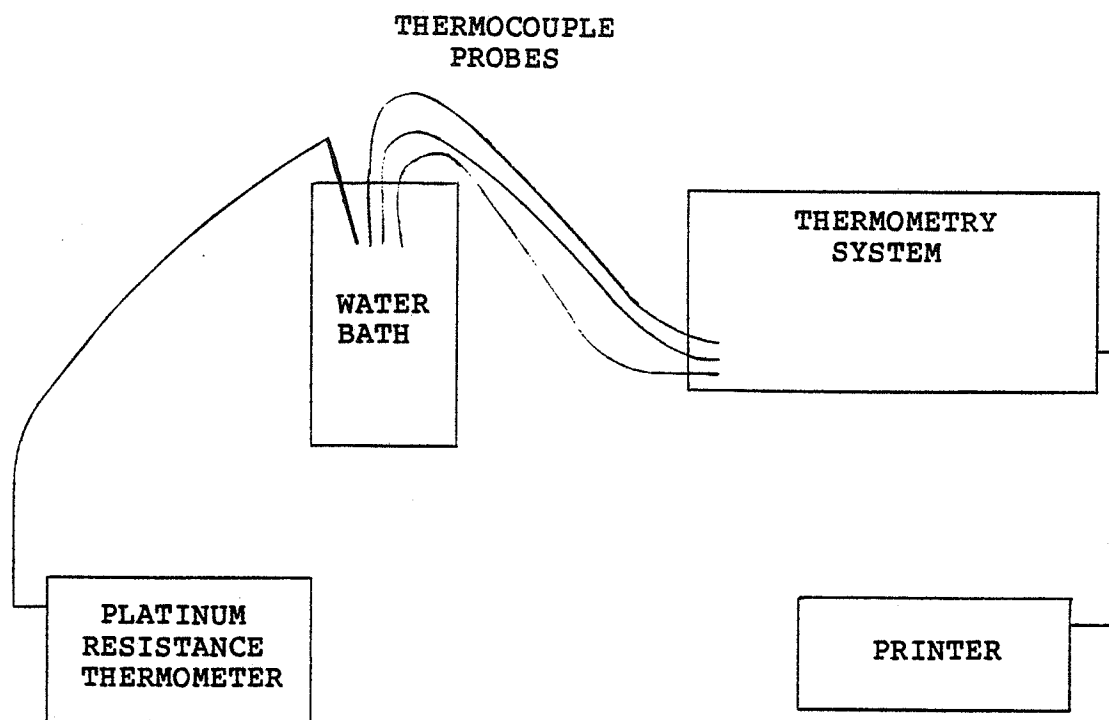


Figure 5.2. Experimental setup for taking data.

Since the water bath takes a moderate amount of time to stabilize, some of the experiments were aided by the use of two water baths.

5.3.2. Accuracy of the Two-Point Calibration

The purpose of this test, which included all the hardware, was to establish that a calibration routine based on two points could work with acceptable accuracy.

In order to set up the most rigid conditions possible, the probes were calibrated at 19.94°C and 59.95°C, which are near the extremes of the valid temperature range. The water bath temperature was then increased from 20°C to 60°C, in steps of about 4°C. At each point, the PRT temperature was read and the probe temperatures were printed out. In Table 5.2 are the PRT temperatures and their corresponding probe output temperatures from the five best channels.

It should be noted that a total of eight channels was observed during this test. However, the intent of the test was to evaluate the performance of the calibration routine only, and probes thought to be in error for some other reason, e.g., hardware failure, were not considered. These other kinds of probe error will be discussed later.

In Figure 5.3, PRT temperature minus thermometry output temperature is plotted versus PRT temperature, for the five best channels. As can be seen, the deviations of thermometry output temperature from PRT temperature are independent of PRT temperature and are concentrated within a range of $\pm 0.03^\circ\text{C}$.

At each PRT temperature in Table 5.2, the mean (average temperature), the standard deviation from the mean and the PRT temperature minus the mean were calculated for the same five

Table 5.2. Thermometry Output at Various Water Bath Temperatures.

PRT (°C)	1 (°C)	5 (°C)	Channel 7 (°C)	8 (°C)	10 (°C)
19.95	19.96	19.96	20.03	20.00	19.99
24.05	24.03	24.05	24.05	24.07	24.07
28.02	27.99	28.00	28.04	28.03	28.02
32.05	31.99	32.02	32.03	32.04	32.05
36.05	36.04	36.03	36.06	36.04	36.05
40.14	40.12	40.12	40.14	40.14	40.17
44.03	44.02	44.01	44.00	44.02	44.03
48.02	48.02	48.01	48.03	48.02	48.03
52.11	52.09	52.10	52.11	52.11	52.11
56.14	56.11	56.13	56.14	56.12	56.14
60.11	60.08	60.07	60.08	60.07	60.08

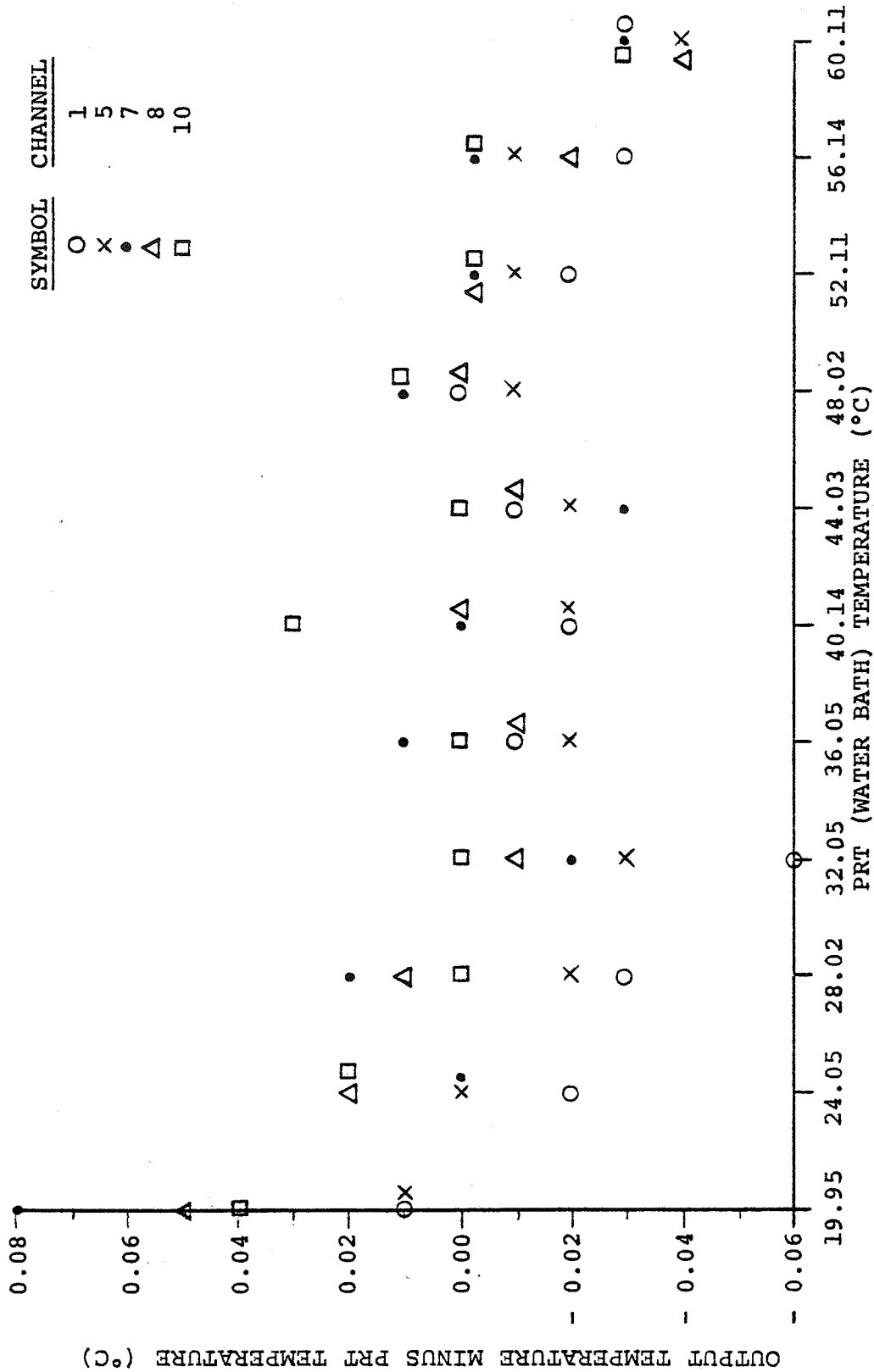


Figure 5.3. Thermometry output temperature minus PRT temperature plotted versus PRT temperature.

channels. These are tabulated in Table 5.3. This estimate of standard deviation is the same as that in Equation (3.3), except now the "ideal temperature" is replaced by the mean. According to the American Society for Testing and Materials (ASTM) [7], accuracy is defined as the degree of agreement between the true value of a property being tested and the average of many observations. The accuracy of the thermometry system is thus represented by the quantity "PRT-MEAN" and, as can be seen, the thermometry system is accurate to within $\pm 0.01^{\circ}\text{C}$ most of the time.

The standard deviation can provide quantitative information on the amount of scatter in the data. The above calculations of standard deviation from the mean will reveal how well localized all the measured temperatures were around their average value. A small value of standard deviation implies a high degree of precision in the measurements, since all the temperatures would be grouped closely together. With this in mind, one can determine an estimate of the precision of the system from the calculated standard deviation. In Table 5.3, the largest value of standard deviation is 0.03°C (rounded to the nearest 0.01°C). The average of all the values of the standard deviation is 0.014°C . Therefore, an estimate of the precision of the system is 0.014°C , with an upper limit of approximately 0.03°C .

This test has demonstrated that the calibration routine will give favorable results over the desired range of calibrated temperatures.

Table 5.3. Channels at Each PRT Temperature.

<u>PRT</u> ($^{\circ}\text{C}$)	<u>Mean</u> ($^{\circ}\text{C}$)	<u>Standard Deviation</u> ($^{\circ}\text{C}$)	<u>(PRT-Mean)</u> ($^{\circ}\text{C}$)
19.95	19.99	0.026	-0.04
24.05	24.05	0.015	0.00
28.02	28.02	0.019	0.00
32.05	32.03	0.021	+0.02
36.05	36.04	0.011	+0.01
40.14	40.14	0.018	0.00
44.03	44.02	0.010	+0.01
48.02	48.02	0.007	0.00
52.11	52.10	0.008	+0.01
56.14	56.13	0.012	+0.01
60.11	60.08	0.005	+0.03

5.3.3. Stability - The Twenty-Four Hour Run

The stability of the thermometry system over long periods of time involves consideration of many factors. For example, it was discovered that the temperature of the water bath could fluctuate by $\pm 0.01^{\circ}\text{C}$ from the desired temperature during long runs. Also, changes in room temperature could have an effect on the internal compensation of the thermocouple amplifier chips. An increase in the ambient chip temperature of only 5°C could cause an error of 0.01°C , as mentioned in Section 3.2.

For this test, the thermometry system was calibrated at 19.97°C and 60.14°C . Then, with the probes in a water bath of about 40.10°C , the output temperatures were sent to the printer every ten minutes for twenty-four hours. Twelve channels were used in this test. Figures 5.4 and 5.5 show the thermometry output temperatures taken every hour for ten of the channels. It is seen that the probe temperatures deviated by -0.07°C to $+0.04^{\circ}\text{C}$ from the PRT temperature of 40.10°C . Channel sixteen's probe was placed inside the thermometry system after a few readings to monitor the temperature of the thermocouple amplifier chips. The output temperatures of probe six all deviated by about 0.16°C from the PRT temperature. This channel's output was not shown on these graphs, but will be considered later.

Figures 5.6 through 5.16 show the variation of temperature every ten minutes for each of the ten channels, including channel six. Notice that most of the channels are fairly well behaved, with the exception of channels five and six. Channel five has one spurious reading, which may have been caused by analog hardware noise, and the readings for channel six are all centered around

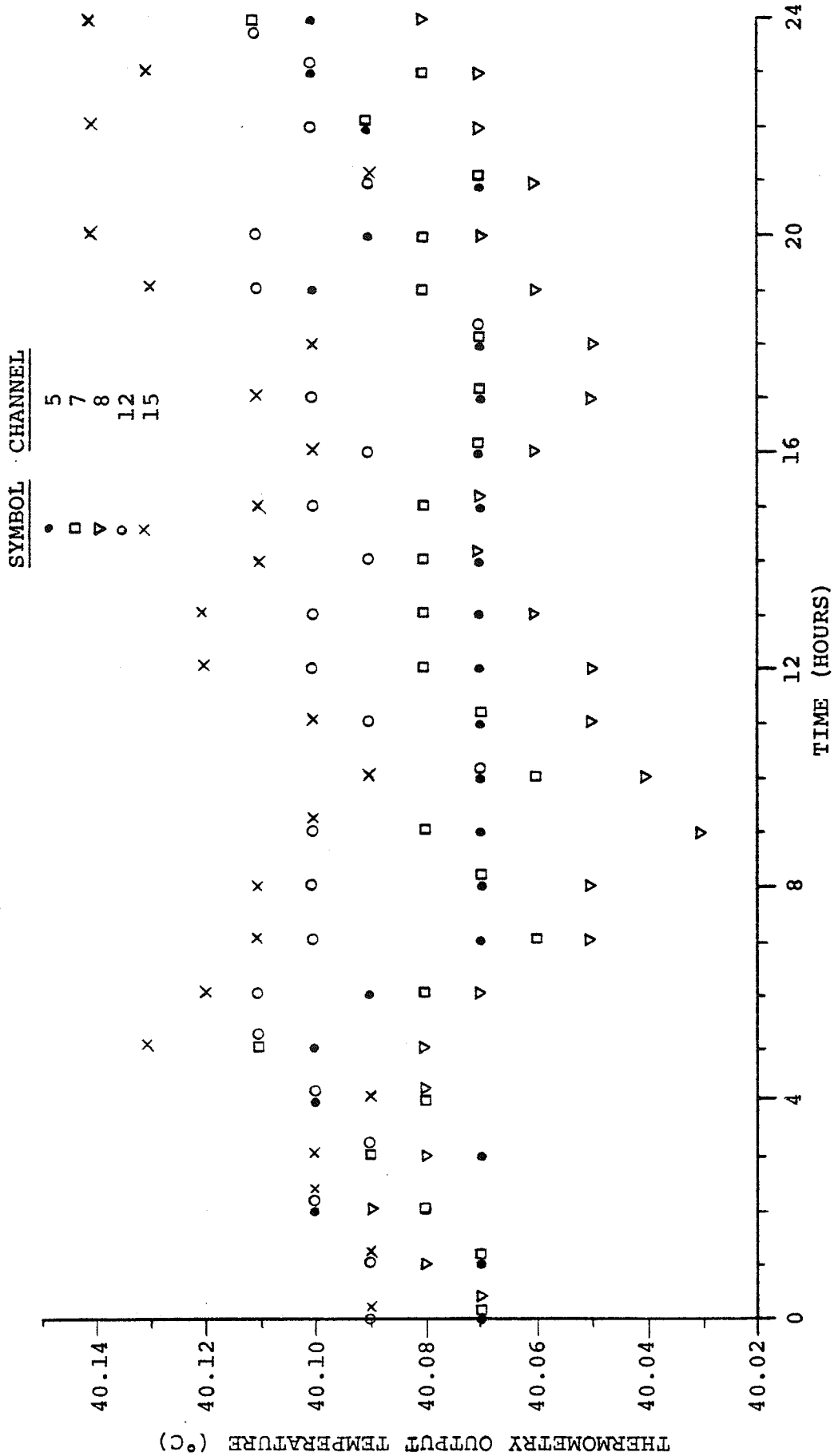


Figure 5.4. Thermometry output over 24 hours with probes in a water bath of 40.10 °C.

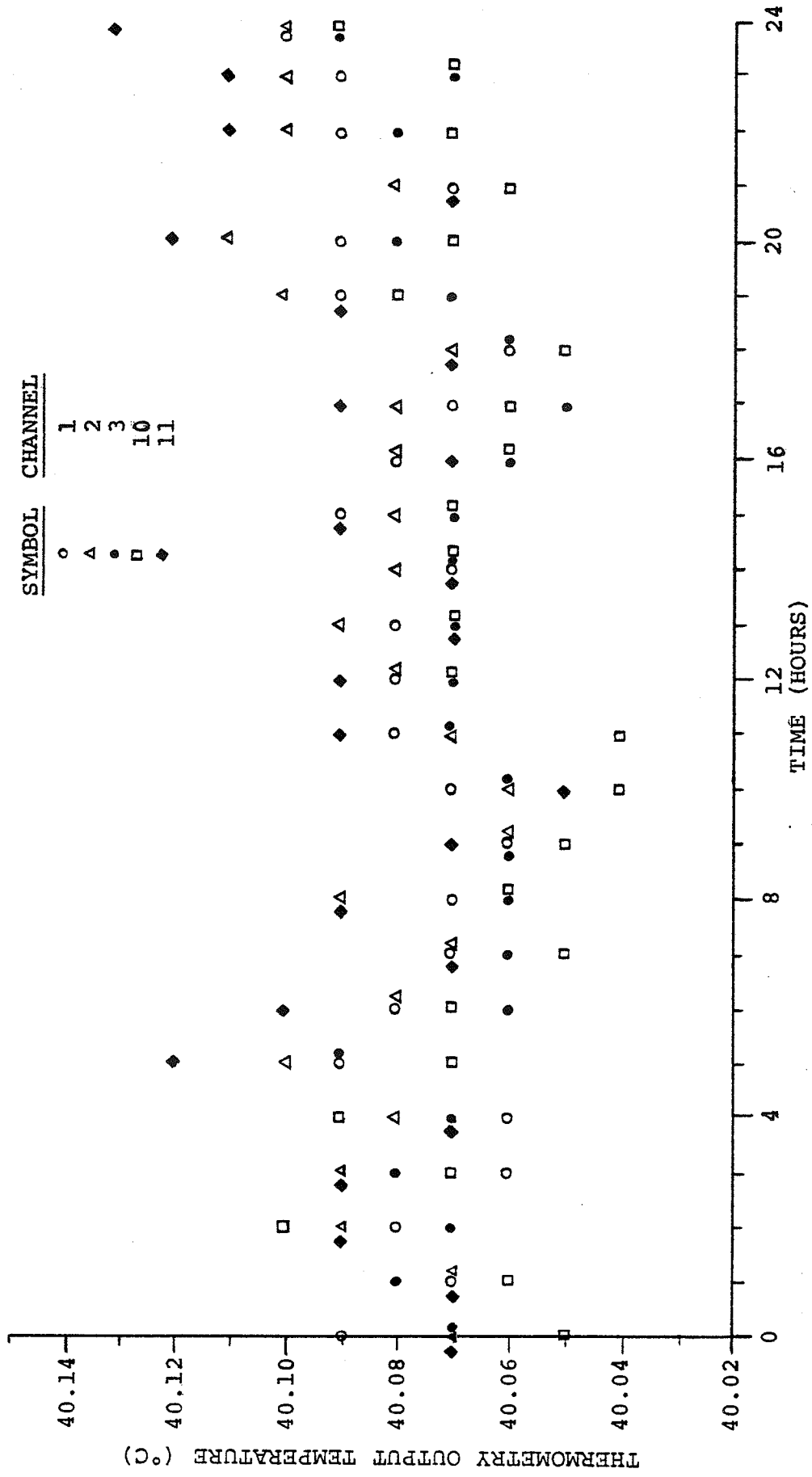


Figure 5.5. Thermometry output over 24 hours with probes in a water bath of 40.10 °C.

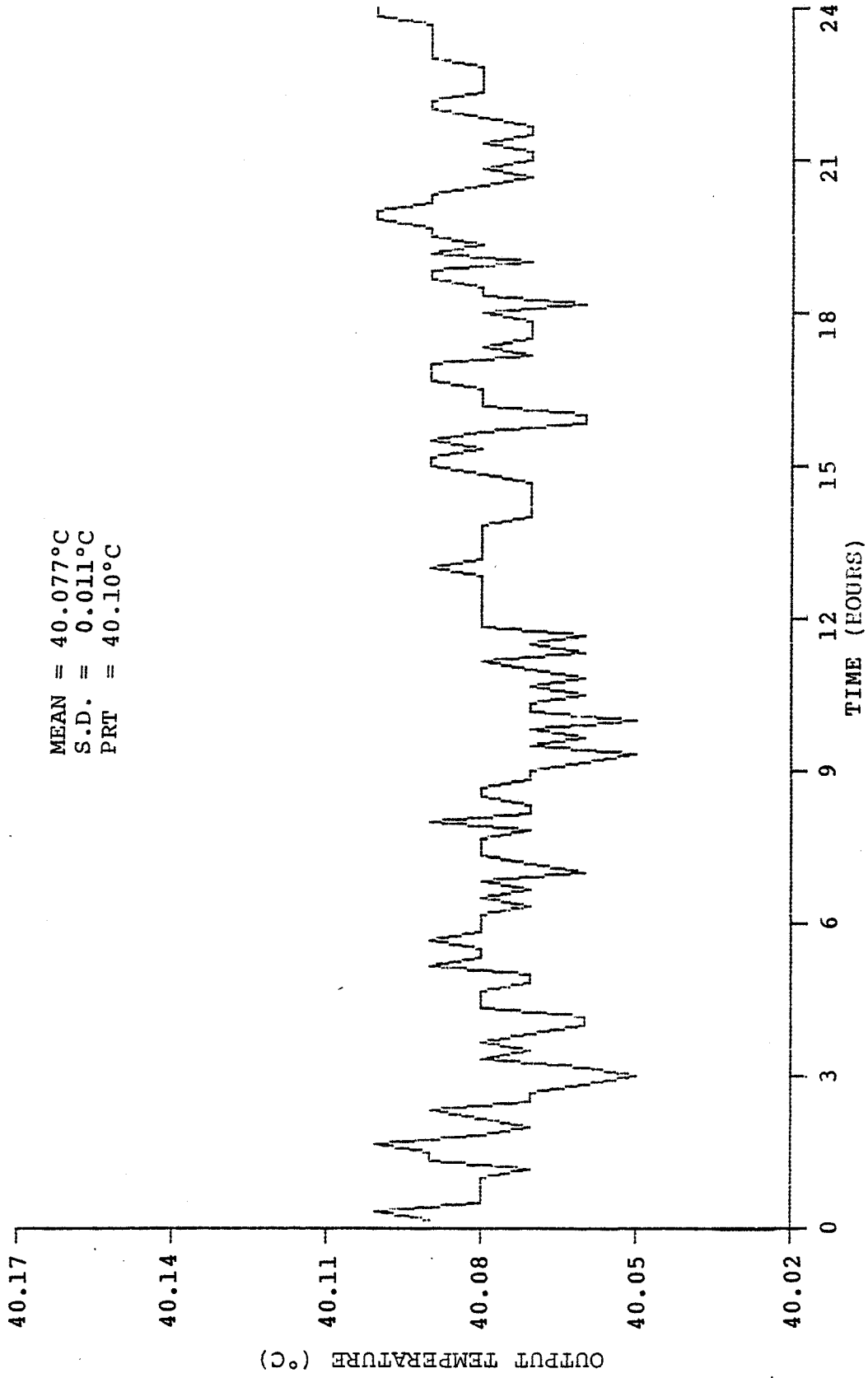


Figure 5.6. Temperature variation of channel 1 with readings made every 10 minutes.

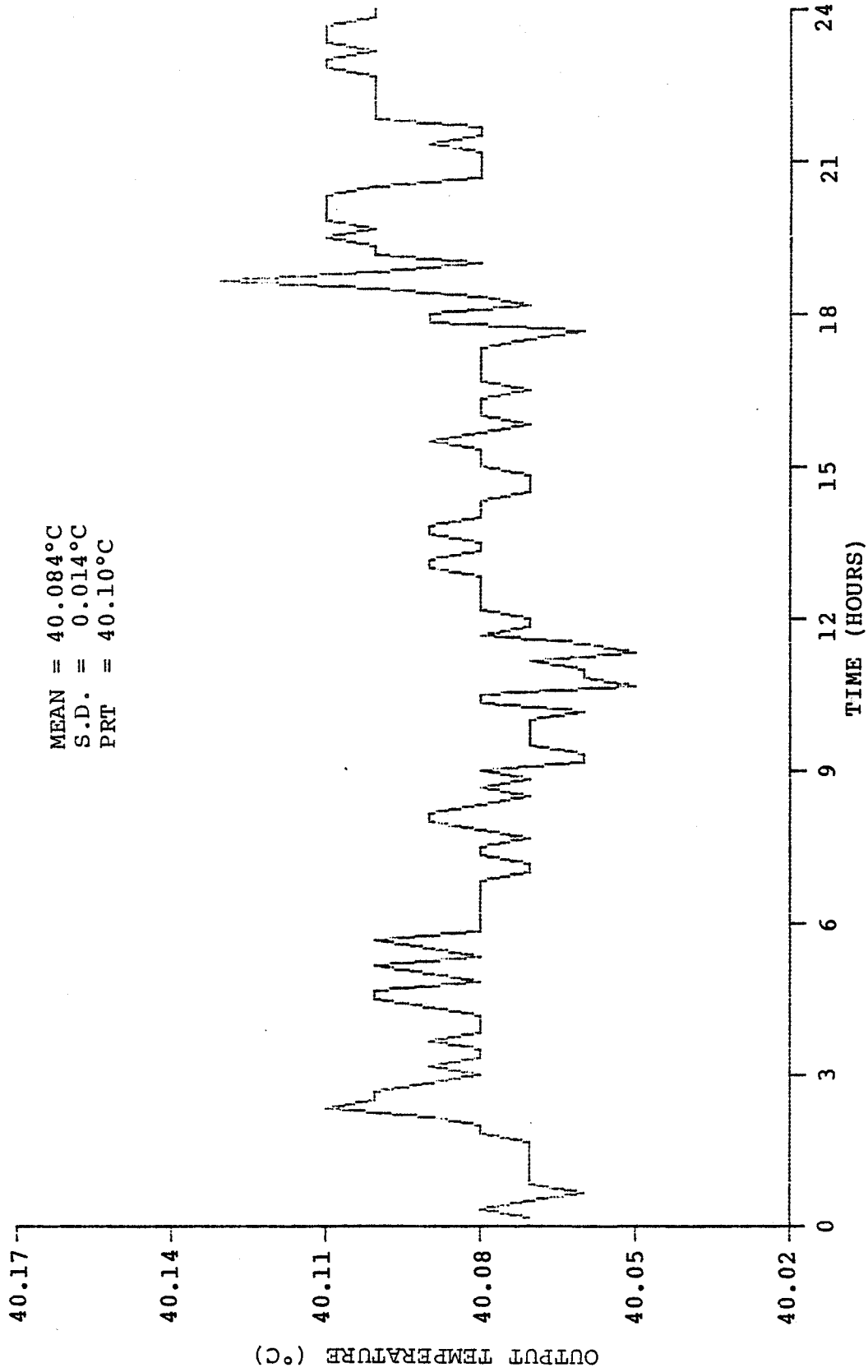


Figure 5.7. Temperature variation of channel 2 with readings made every 10 minutes.

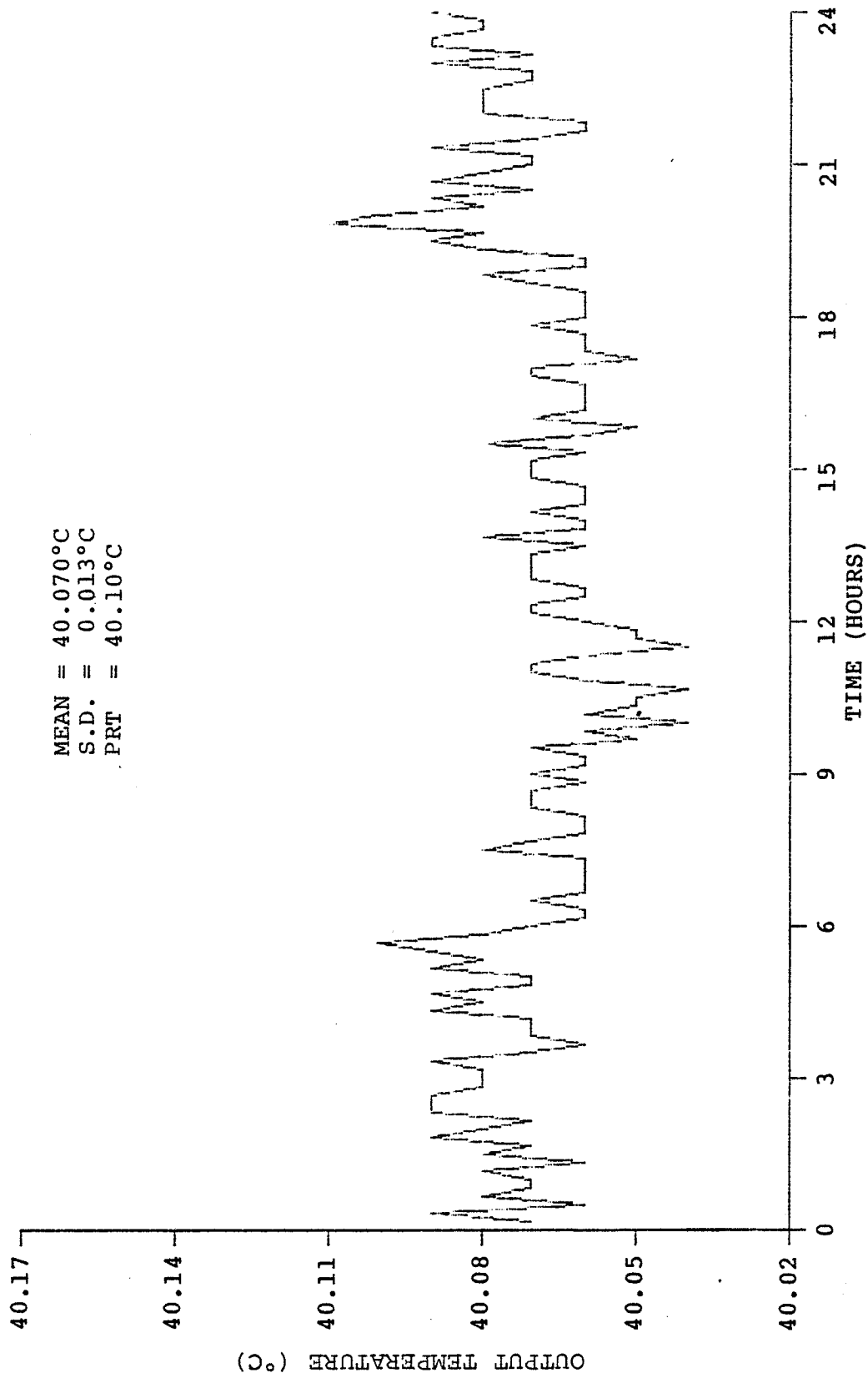


Figure 5.8. Temperature variation of channel 3 with readings made every 10 minutes.

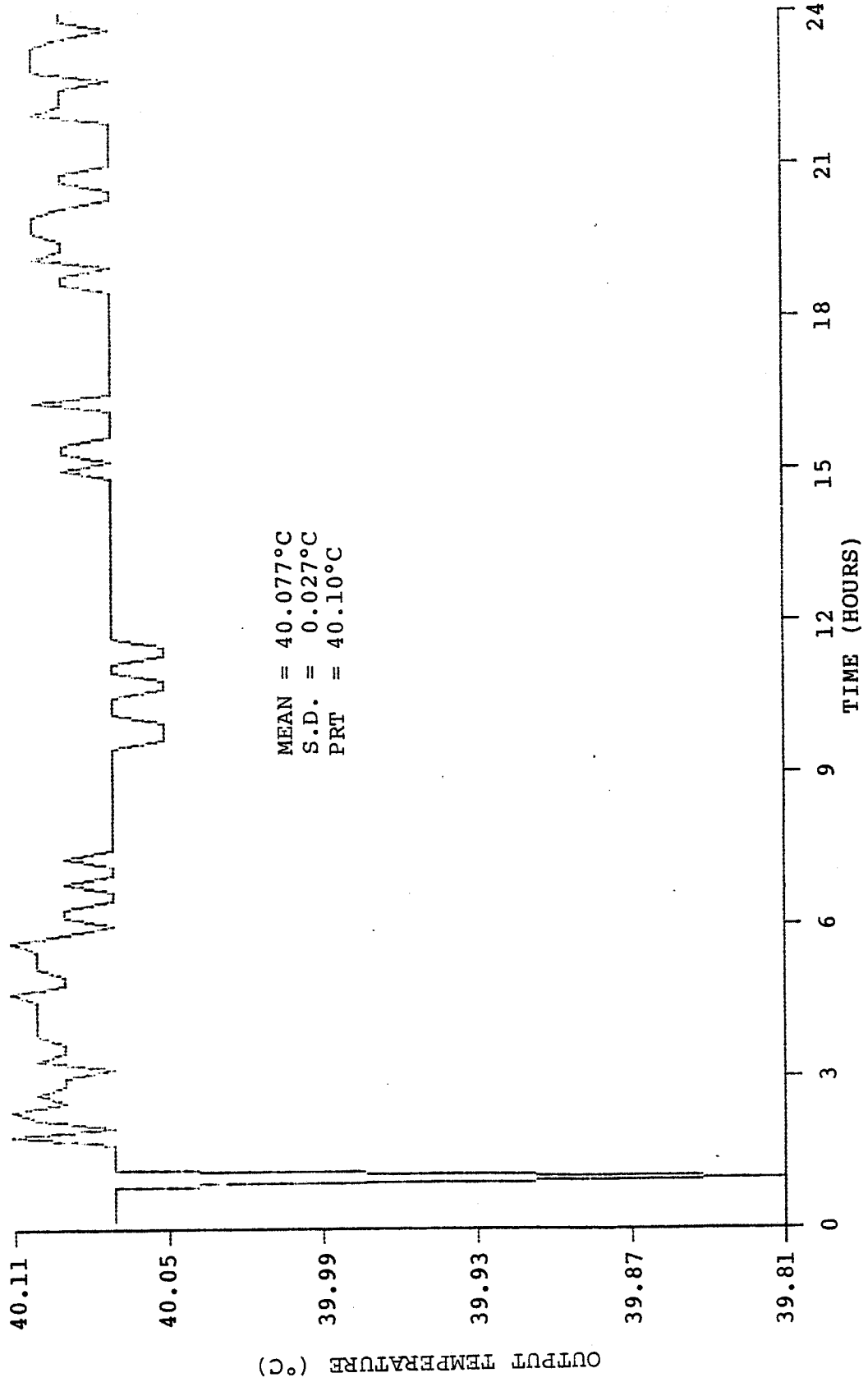


Figure 5.9. Temperature variation of channel 5 with readings made every 10 minutes.

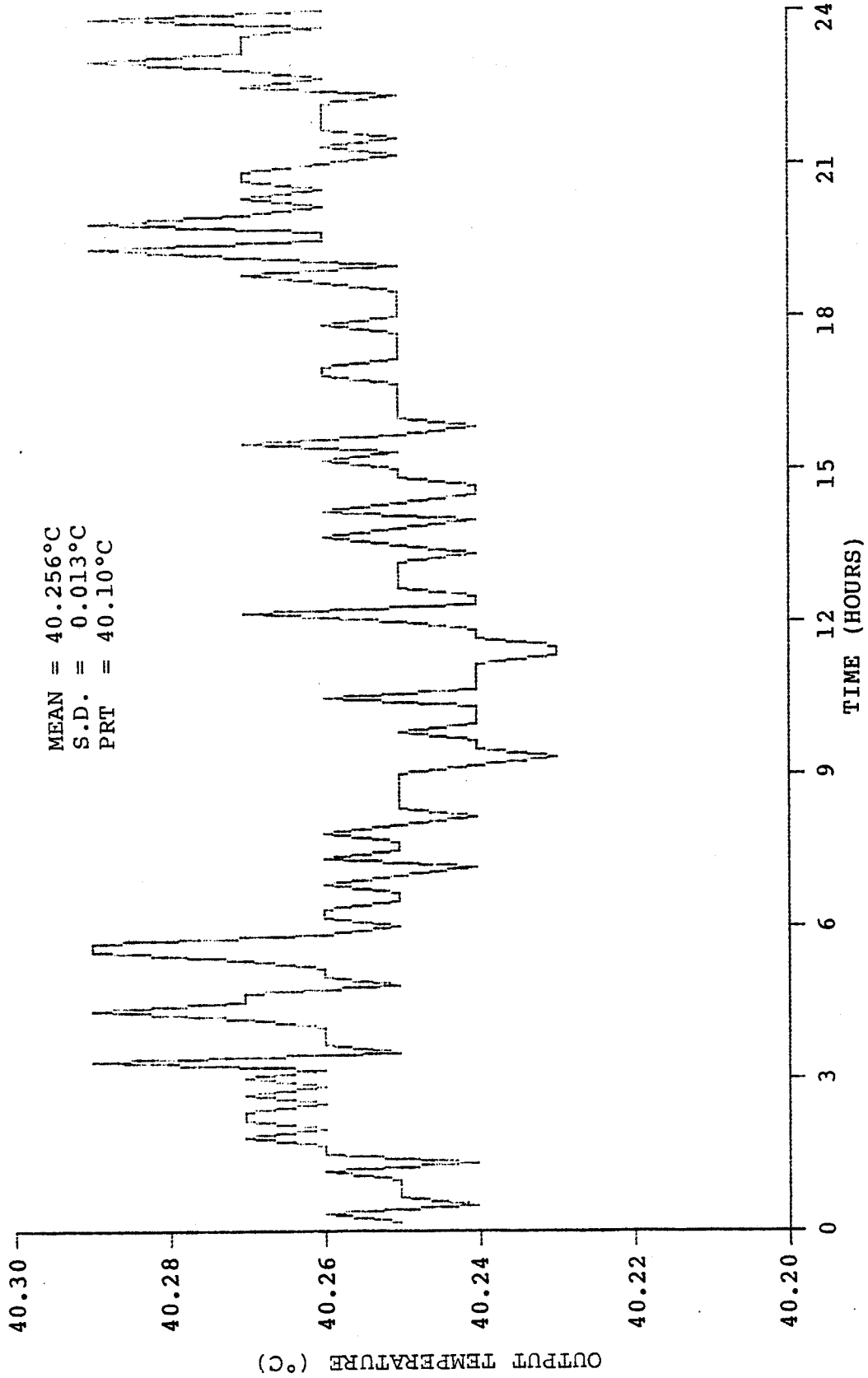


Figure 5.10. Temperature variation of channel 6 with readings made every 10 minutes.

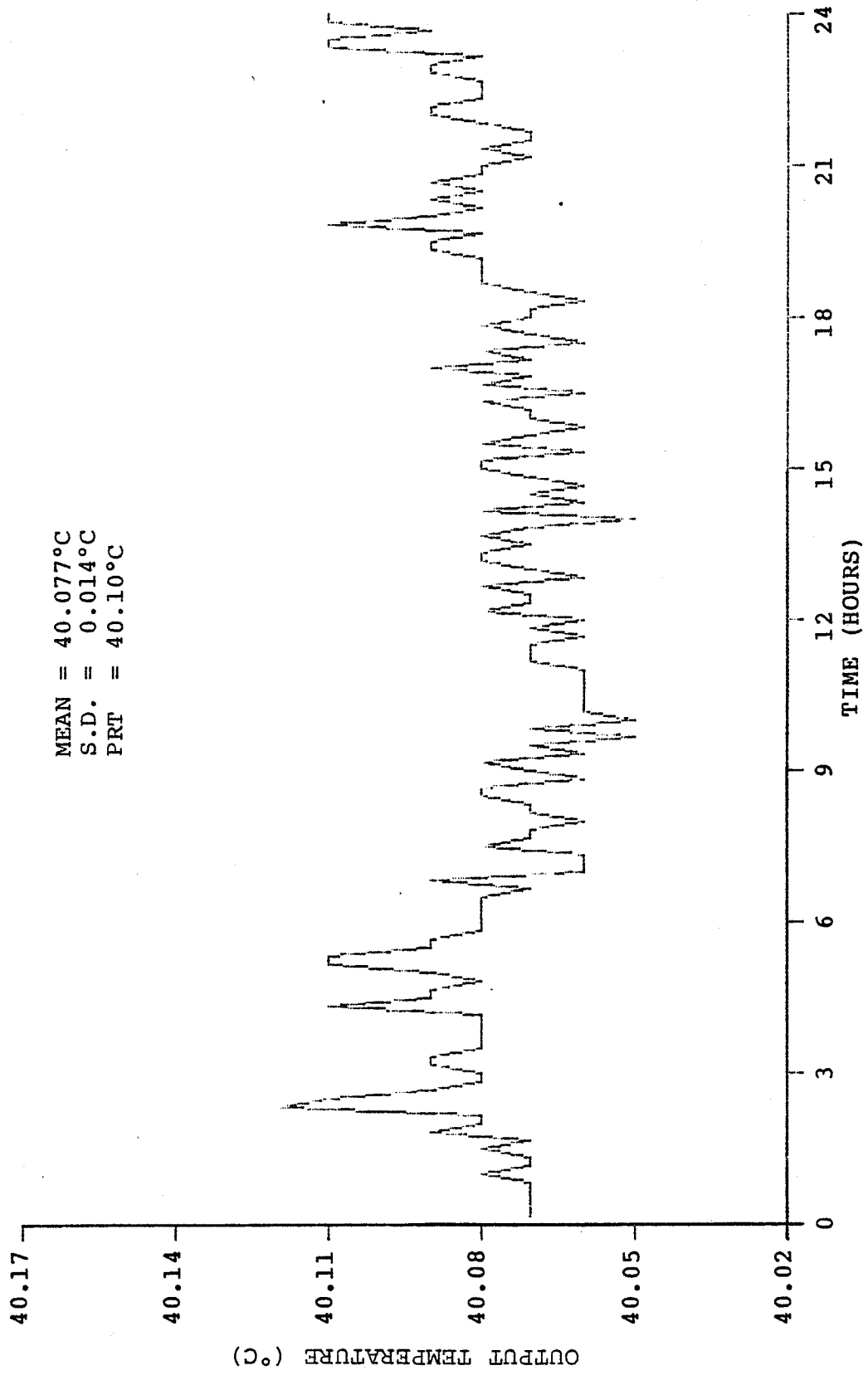


Figure 5.11. Temperature variation of channel 7 with readings made every 10 minutes.

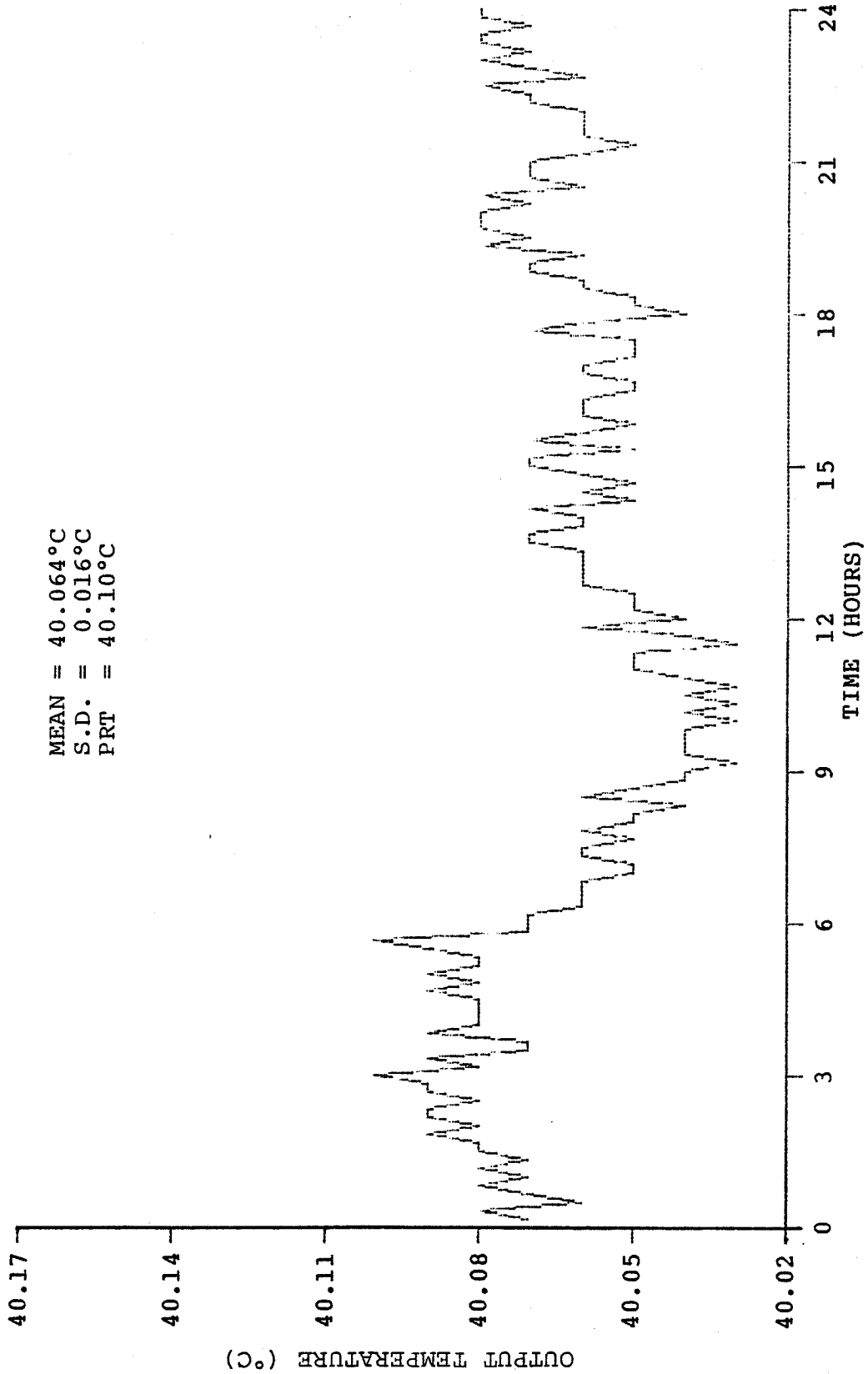


Figure 5.12. Temperature variation of channel 8 with readings made every 10 minutes.

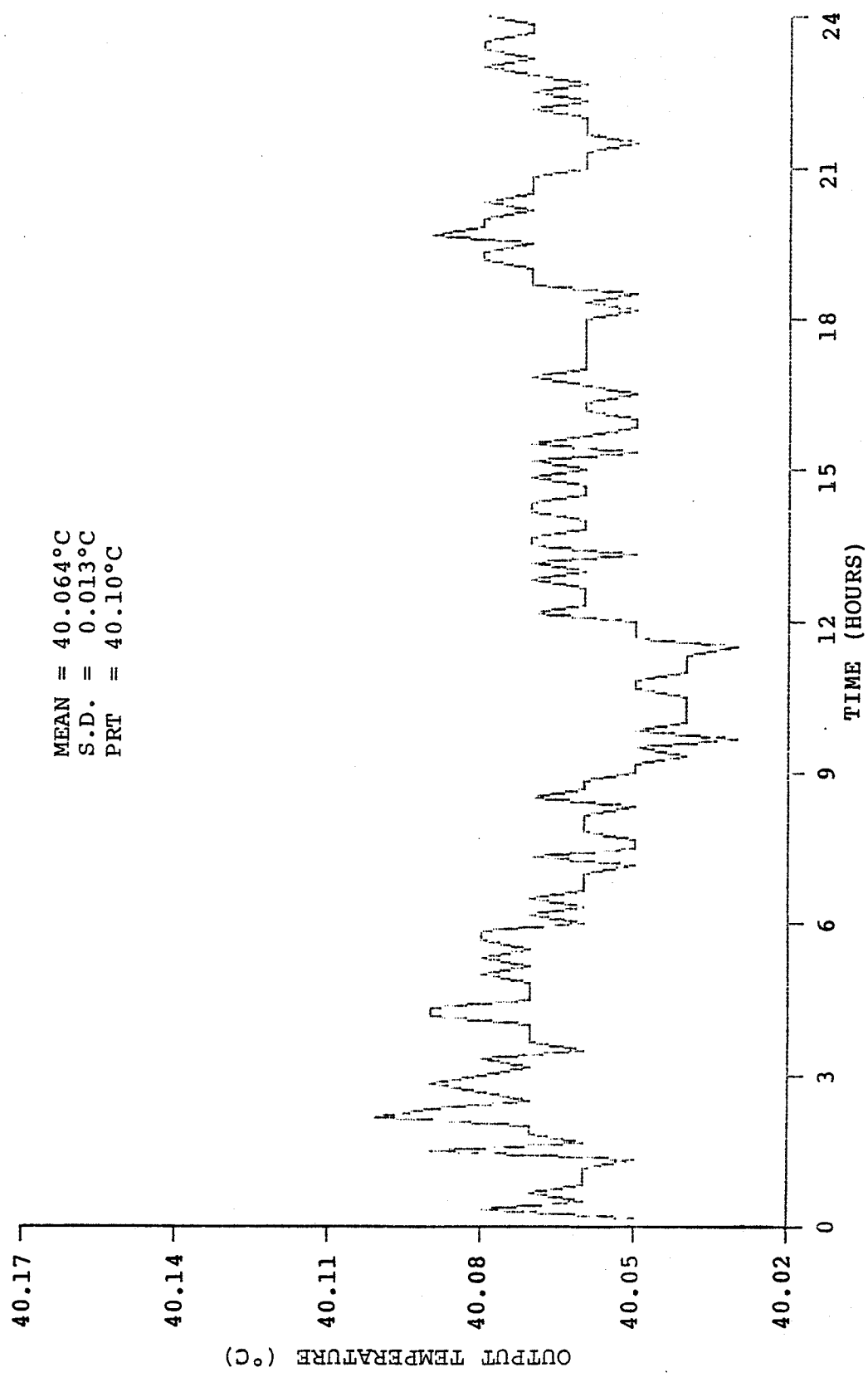


Figure 5.13. Temperature variation of channel 10 with readings made every 10 minutes.

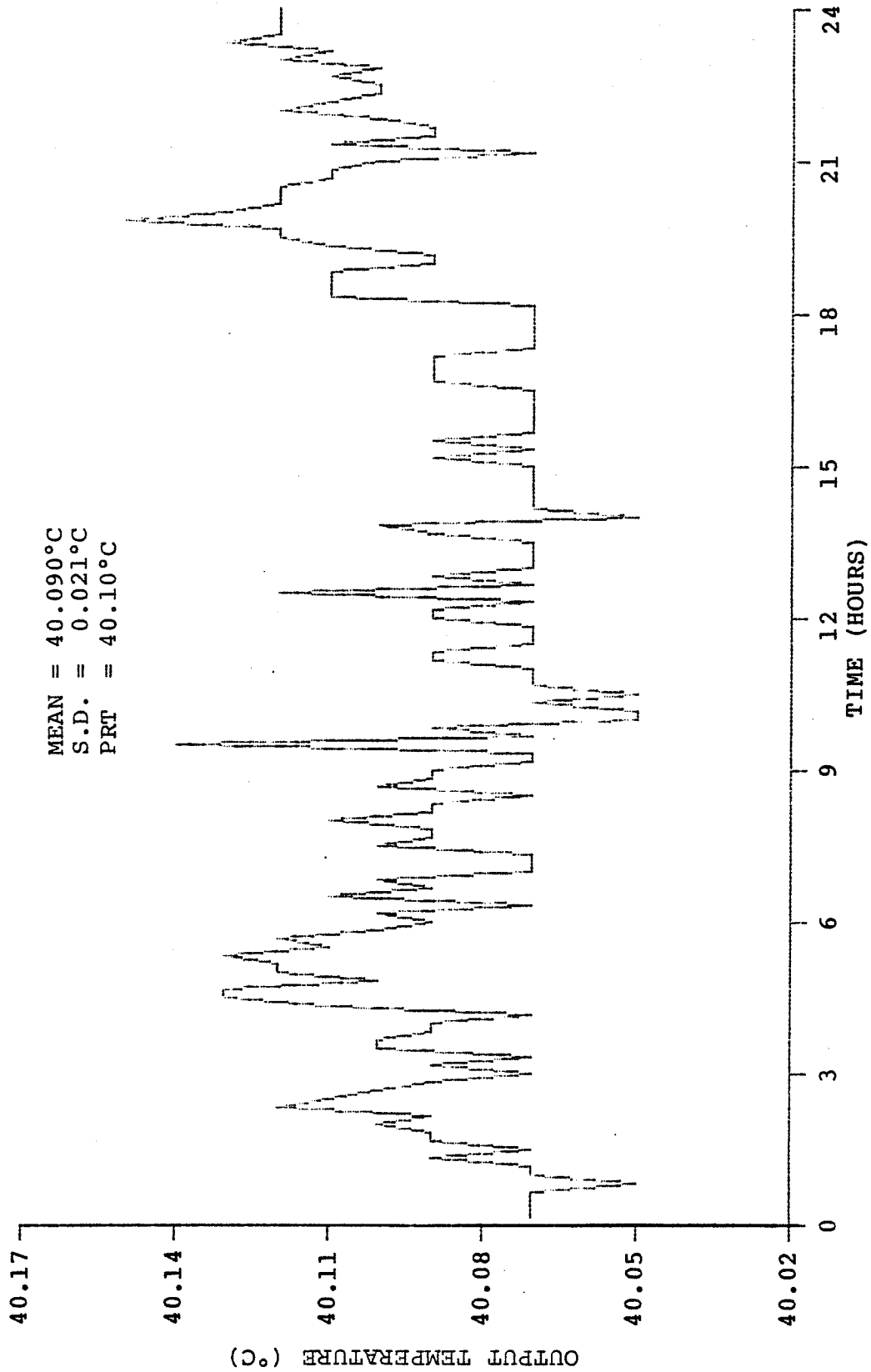


Figure 5.14. Temperature variation of channel 11 with readings made every 10 minutes.

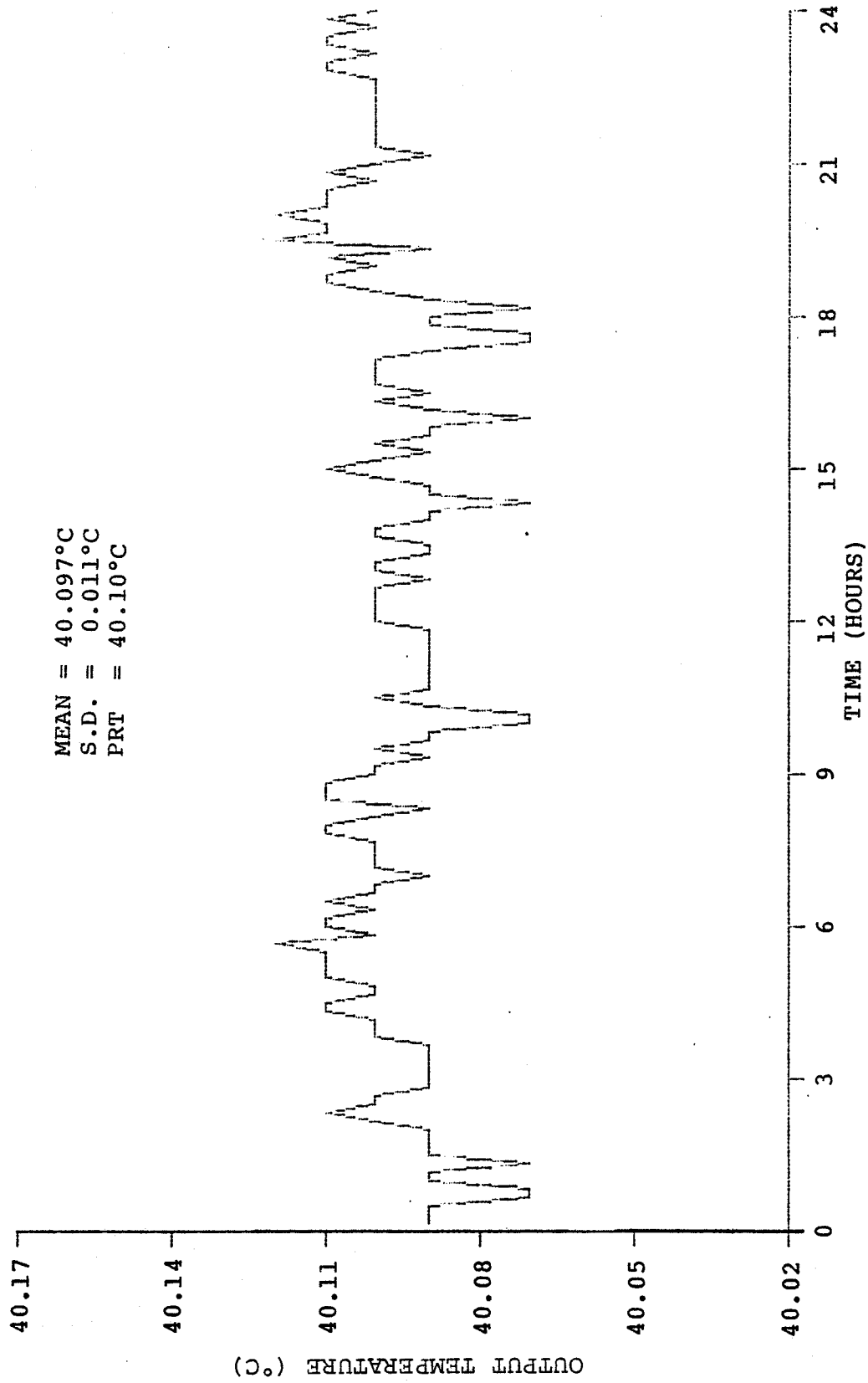


Figure 5.15. Temperature variation of channel 12 with readings made every 10 minutes.

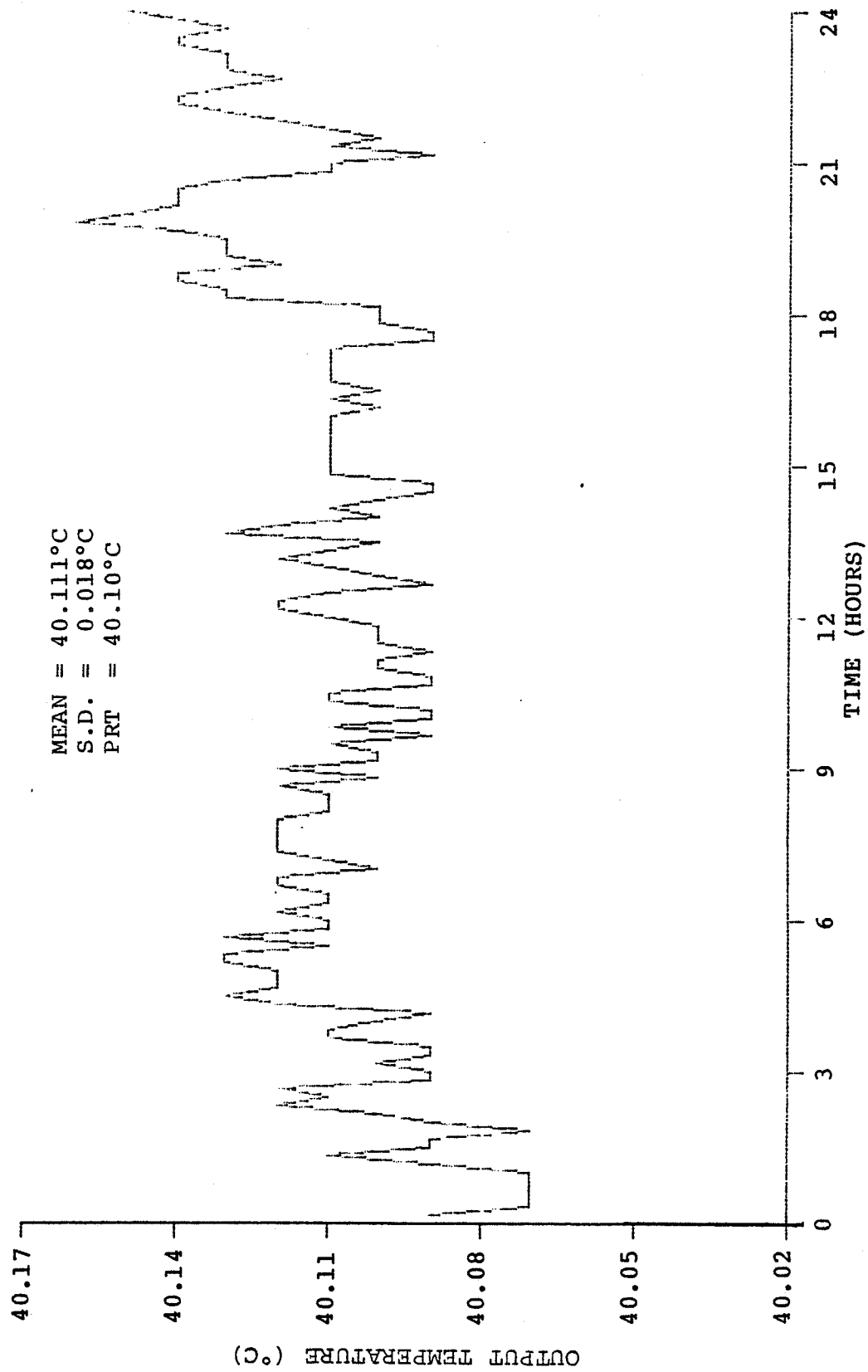


Figure 5.16. Temperature variation of channel 15 with readings made every 10 minutes.

40.26°C. Also, the mean and standard deviation for each channel are printed on the graphs and tabulated in Table 5.4.

Comparing the mean values to the PRT value of 40.10°C will give a measure of the accuracy of the thermometry system, as discussed in the previous subsection. As seen in Table 5.4, all channels, except channel six, are accurate to within $\pm 0.04^\circ\text{C}$. However, all the channels are precise. The standard deviation, which is a measure of the precision, is less than 0.03°C for all channels.

5.3.5. Repeatability

The repeatability of accurate, calibrated temperatures was examined in a series of structured tests. Before each of the twelve experiments, described in Table 5.5, a calibration was performed at approximately 20°C and 60°C . Then, the probes were read at particular intervals of time while in a constant temperature water bath, stable to within $\pm 0.01^\circ\text{C}$.

Twelve channels were used in each test. For a particular test, all twelve channels were read at each reading. The output temperatures of all twelve channels were then plotted together in the form of a histogram. For the tests where 100 readings were made, twenty representative readings were chosen from each channel. Therefore, each histogram contains $20 * 12 = 240$ data points, which represents twenty temperature readings from each of the twelve channels. Figures 5.17 through 5.28 are the point histograms plotting the number of times each temperature occurs versus temperature, for each test. Also, the PRT temperature and the mean temperature have been marked on the plots. This method of presenting the data gives additional insight into the

Table 5.4. Properties of Each Channel in the Twenty-four Hour Run.

<u>Channel</u>	<u>Mean(°C)</u>	<u>Standard Deviation(°C)</u>	<u>(40.1°C-Mean) (°C)</u>
1	40.08	0.011	+0.02
2	40.08	0.014	+0.02
3	40.07	0.013	+0.03
5	40.08	0.027	+0.02
6	40.26	0.013	-0.16
7	40.08	0.014	+0.02
8	40.06	0.016	+0.04
10	40.06	0.013	+0.04
11	40.09	0.021	+0.01
12	40.10	0.011	0.00
15	40.11	0.018	-0.01

Table 5.5. Format of the Twelve Tests.

<u>Test Number</u>	<u>Temperature of Water Bath(°C)</u>	<u>Time Between Reading(sec)</u>	<u>Number of Readings</u>
1	20	10	20
2	20	36	100
3	20	60	20
4	20	180	100
5	40	10	20
6	40	36	100
7	40	60	20
8	40	180	100
9	60	10	20
10	60	36	100
11	60	60	20
12	60	180	100

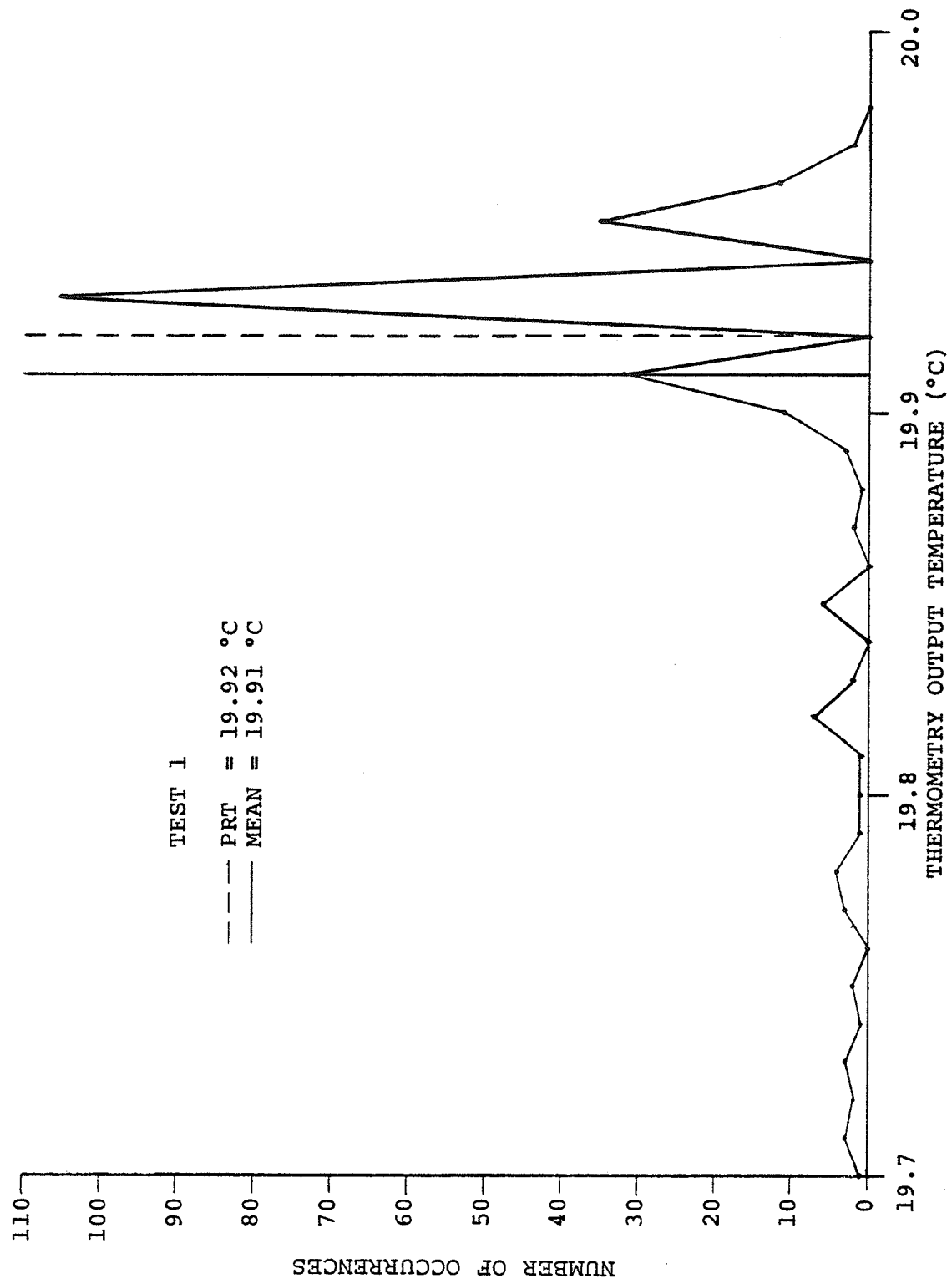


Figure 5.17. Distribution of output temperatures when probes are read every 10 seconds.

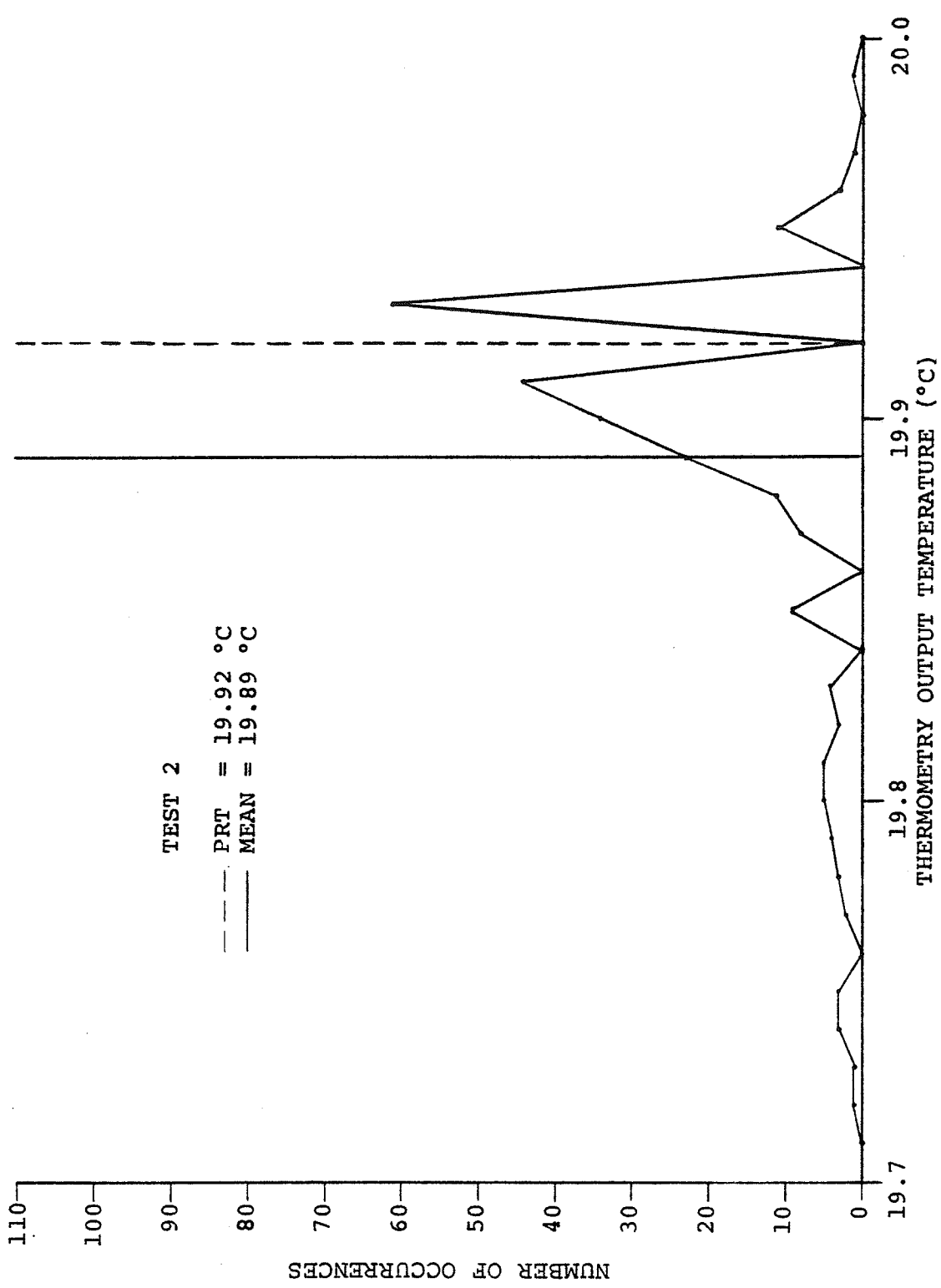


Figure 5.18. Distribution of output temperatures when probes are read every 36 seconds.

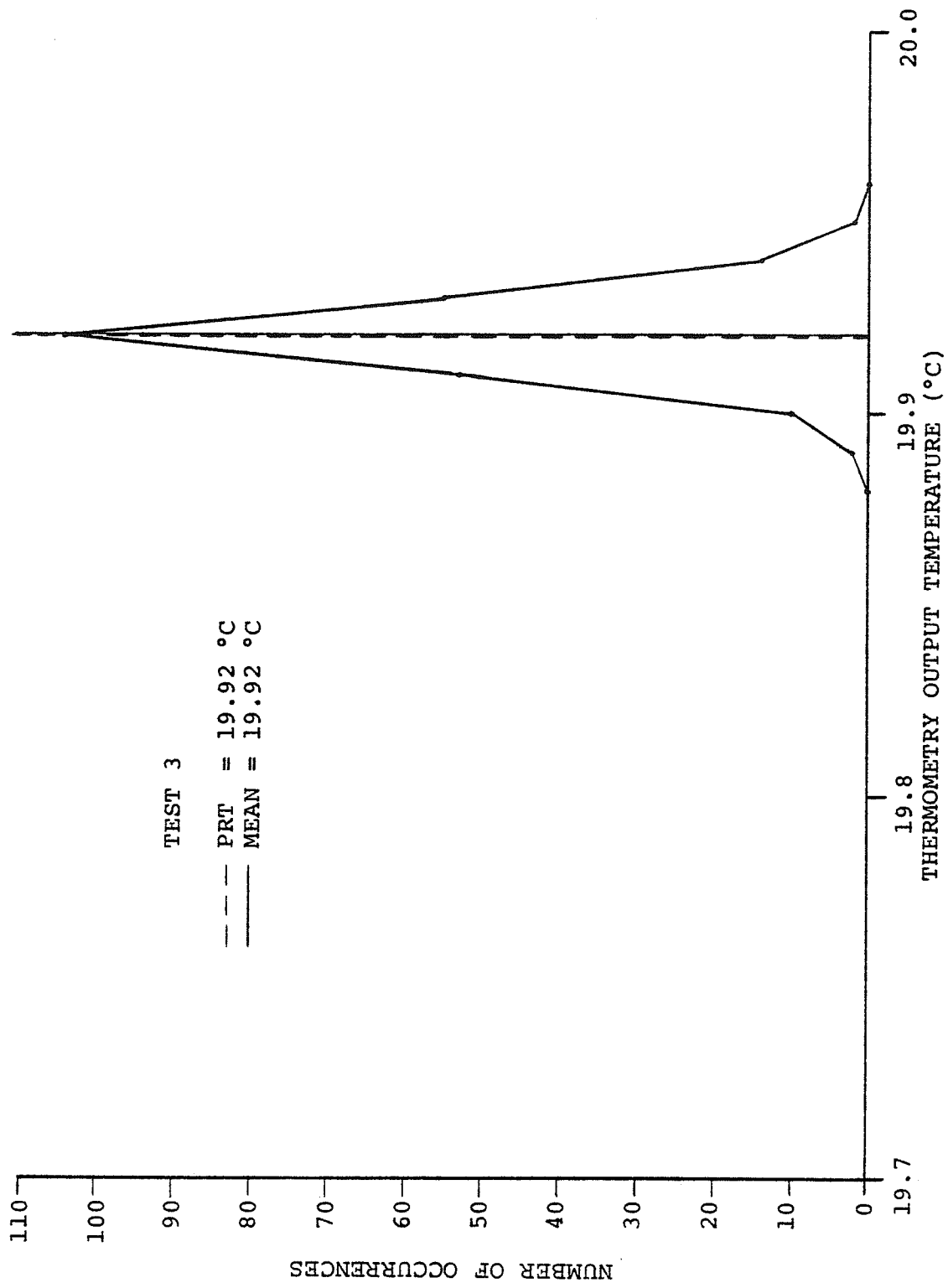


Figure 5.19. Distribution of output temperature when probes are read every 60 seconds.

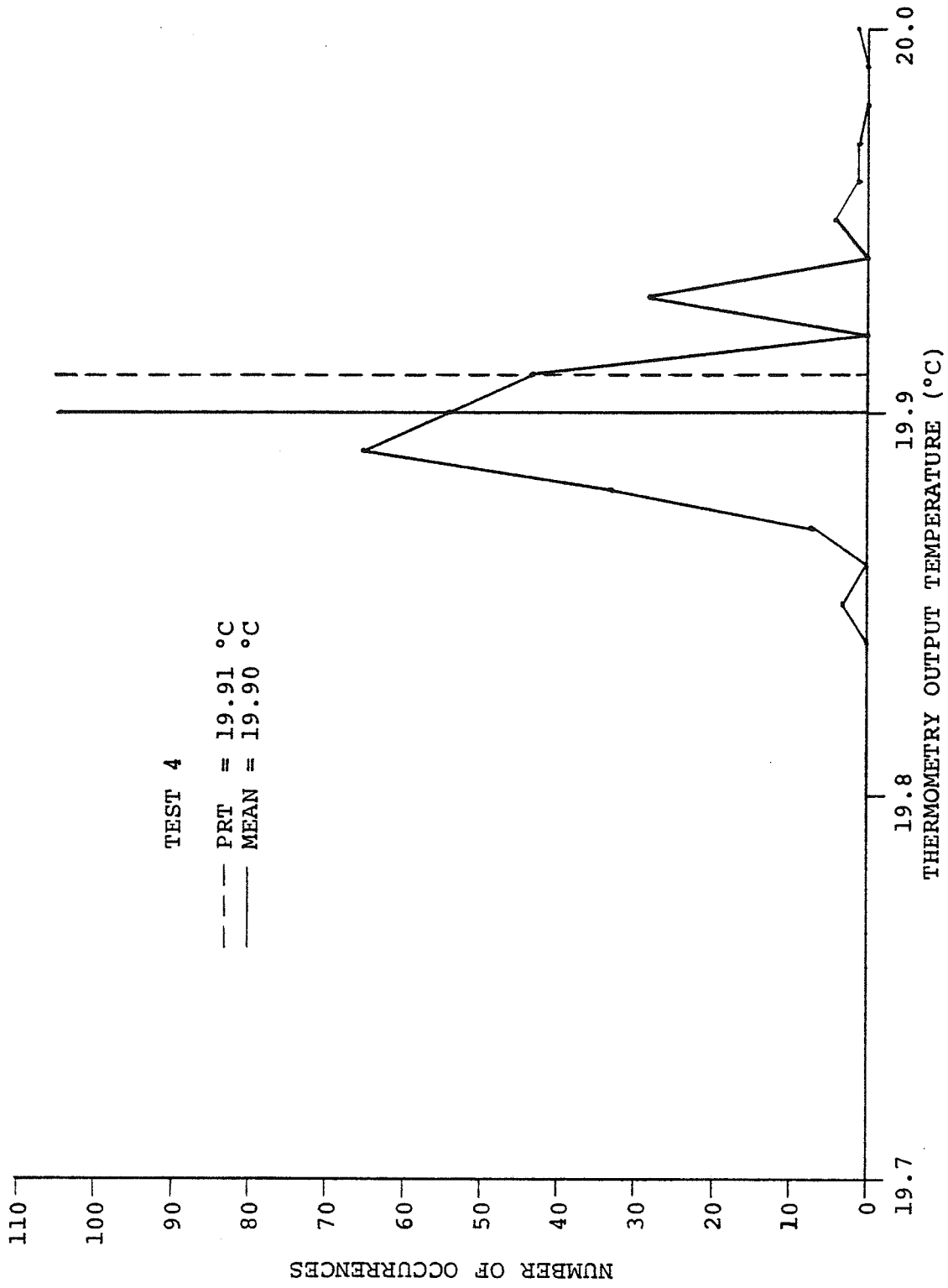


Figure 5.20. Distribution of output temperatures when probes are read every 180 seconds.

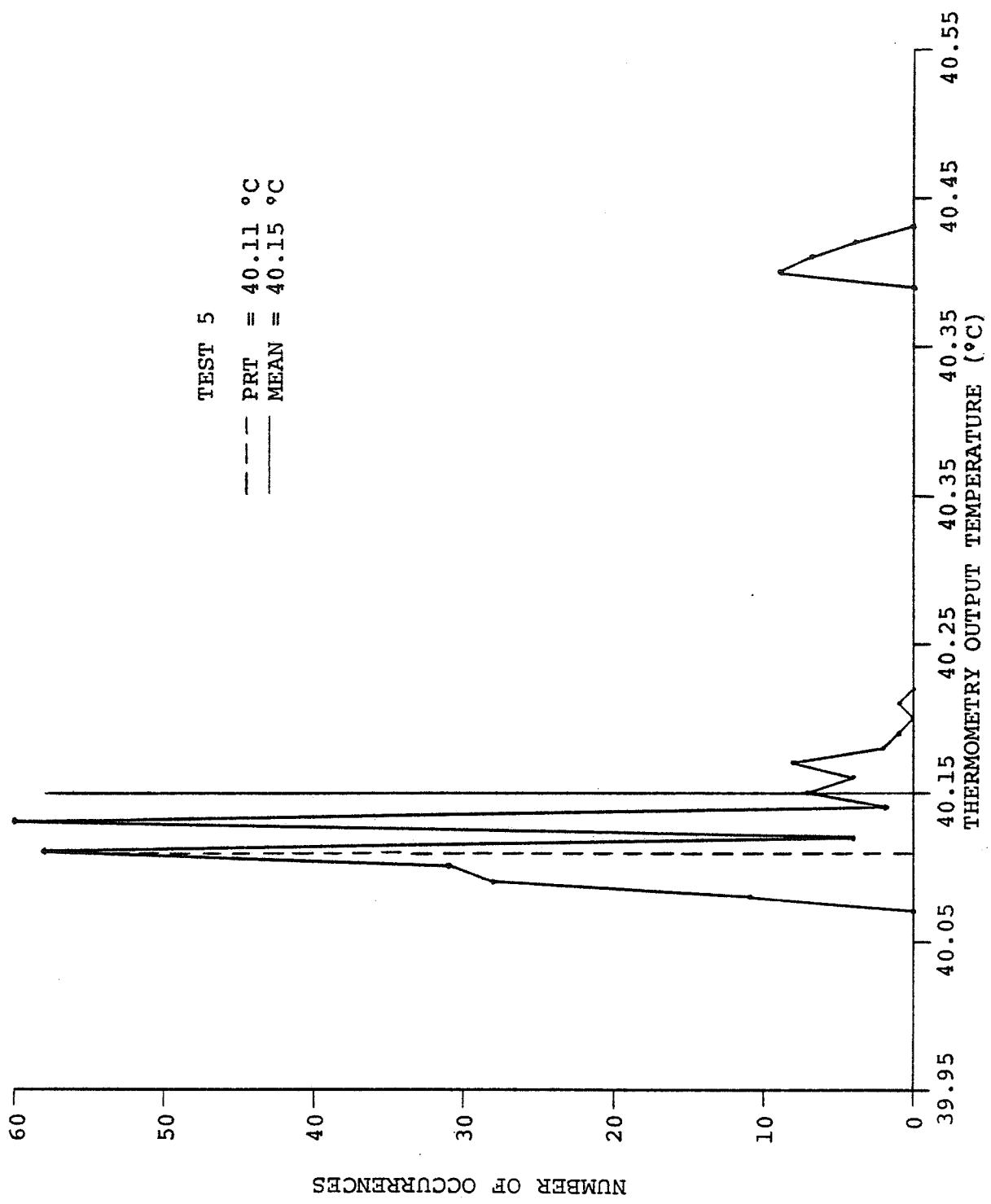


Figure 5.21. Distribution of output temperatures when probes are read every 10 seconds.

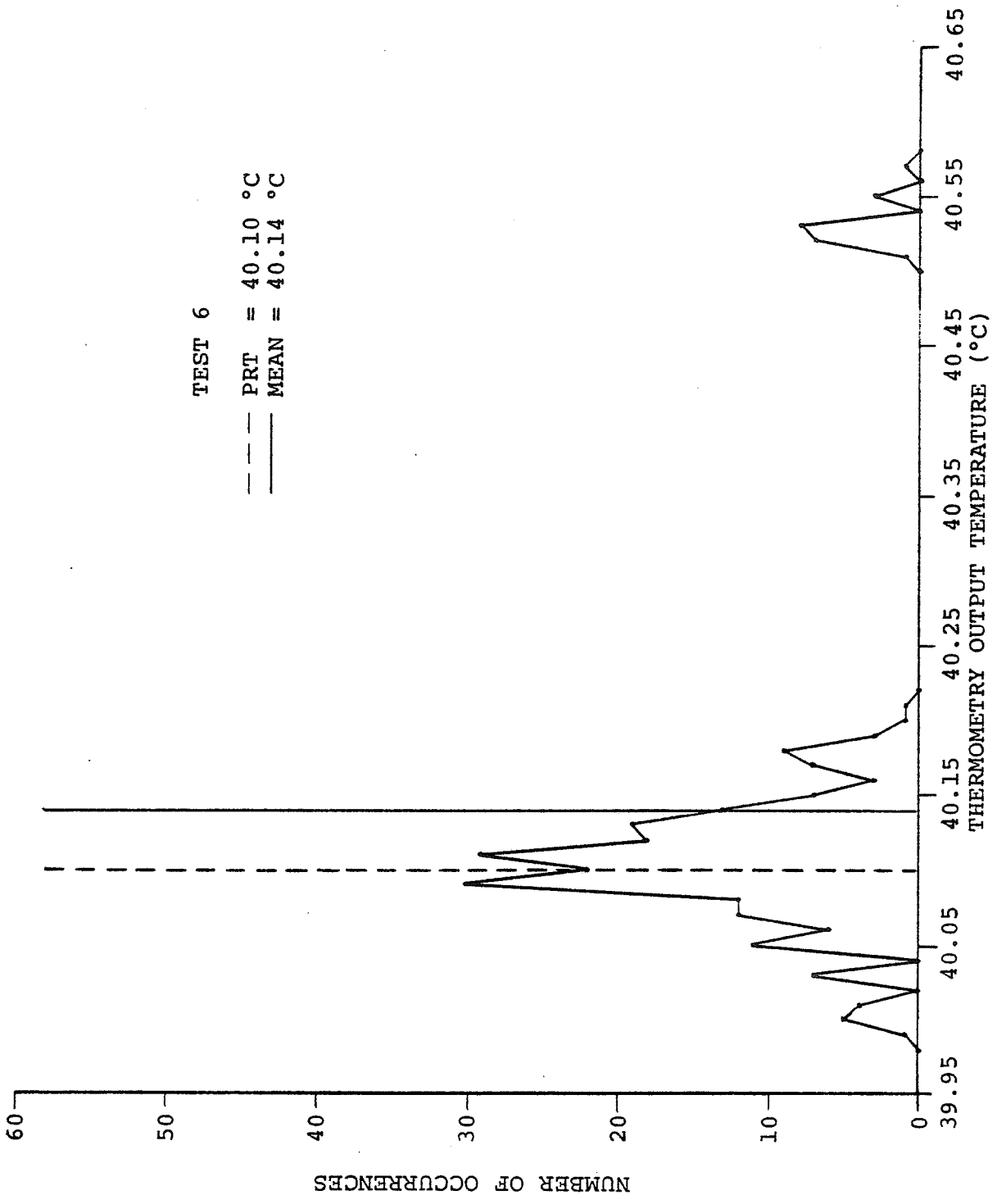


Figure 5.22. Distribution of output temperatures when probes are read every 36 seconds.

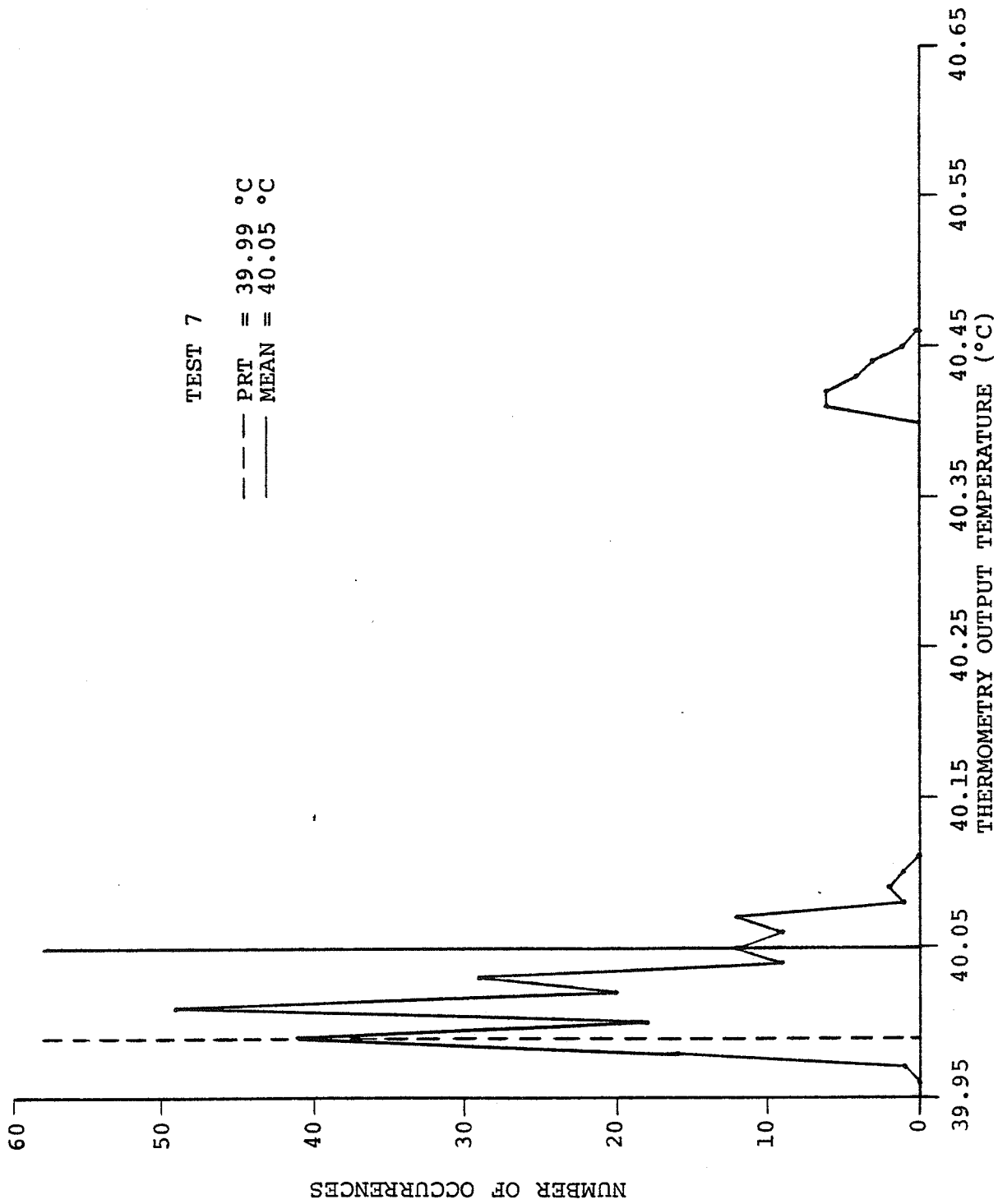


Figure 5.23. Distribution of output temperatures when probes are read every 60 seconds.

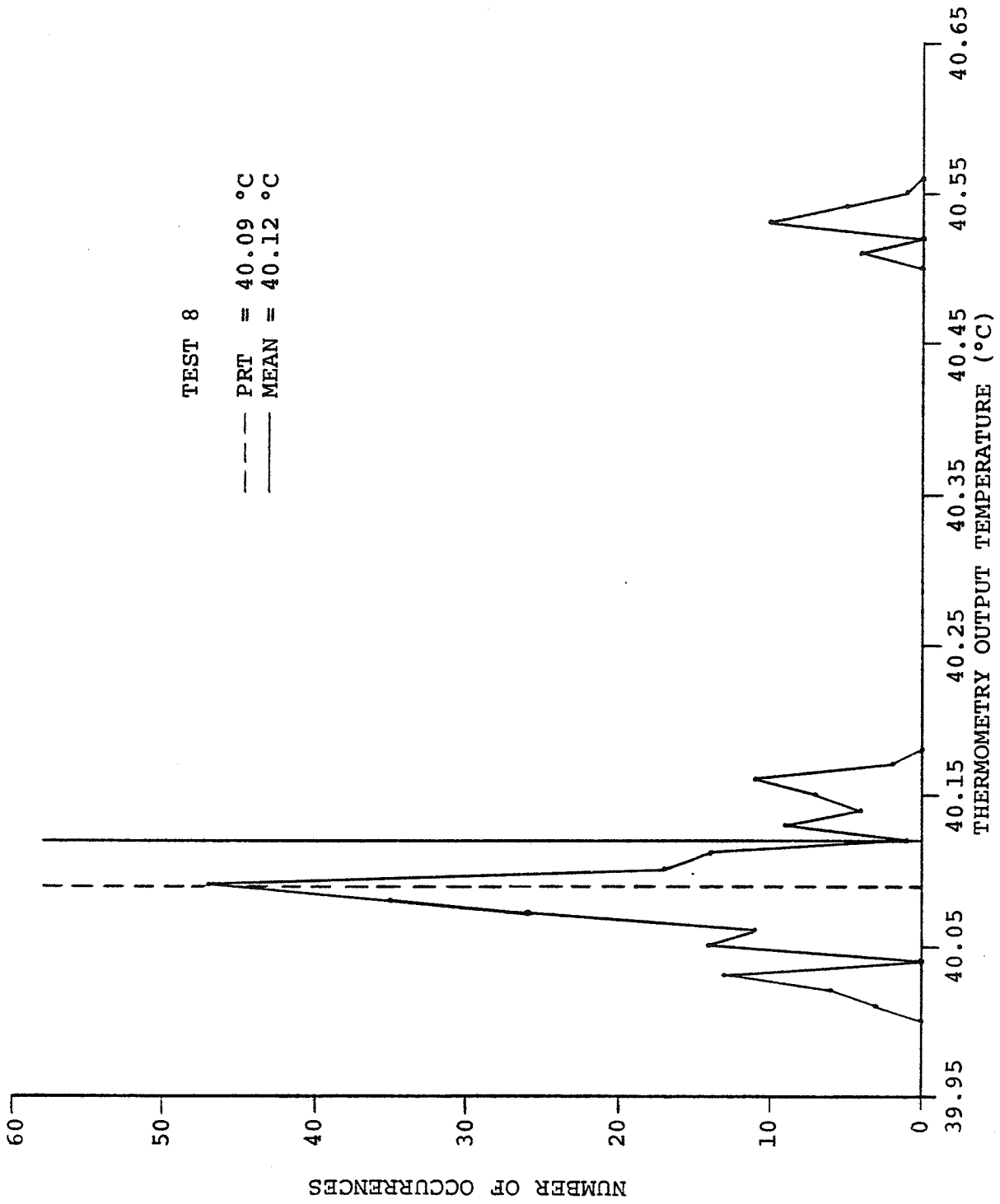


Figure 5.24. Distribution of output temperatures when probes are read every 180 seconds.

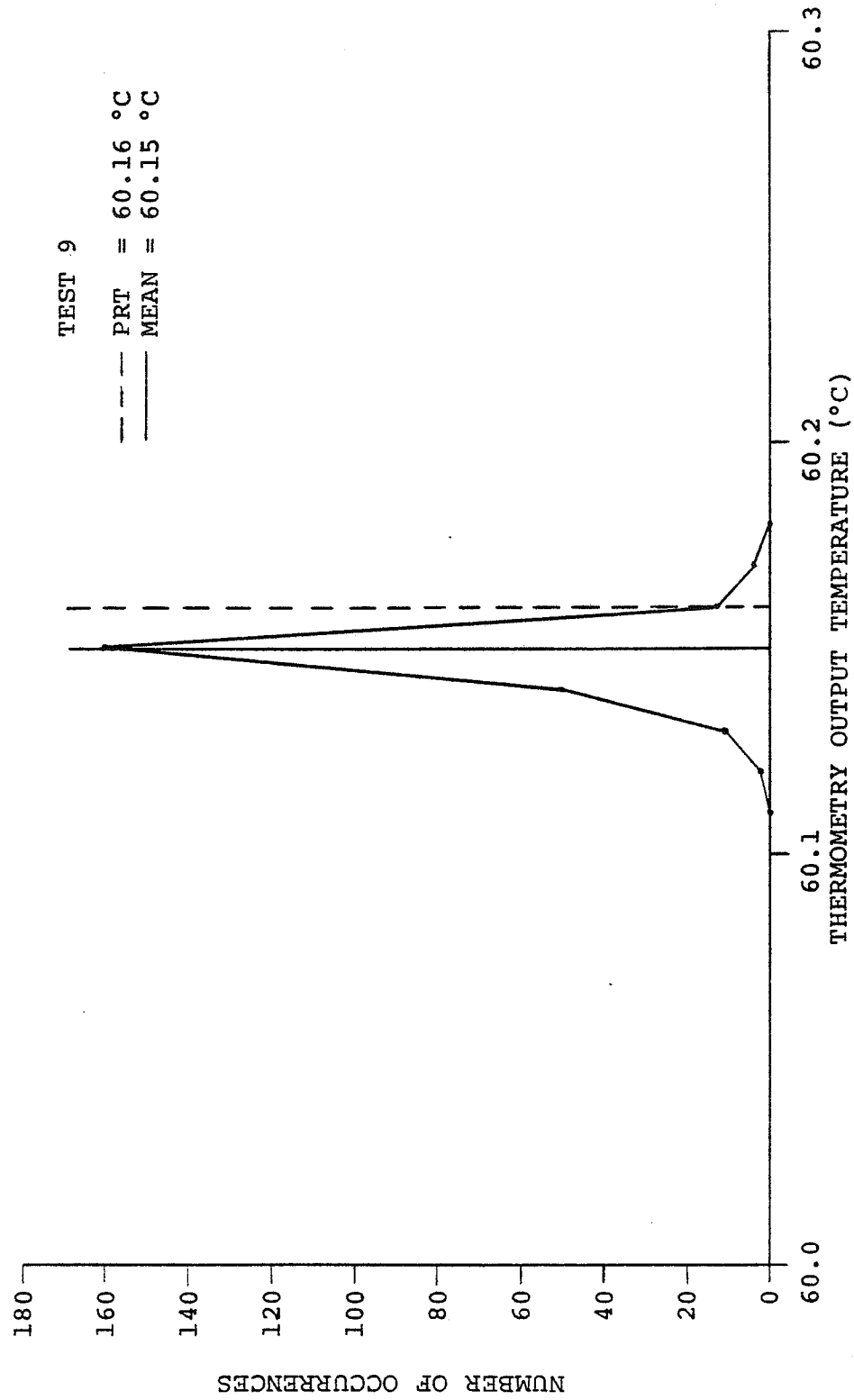


Figure 5.25. Distribution of output temperatures when probes are read every 10 seconds.

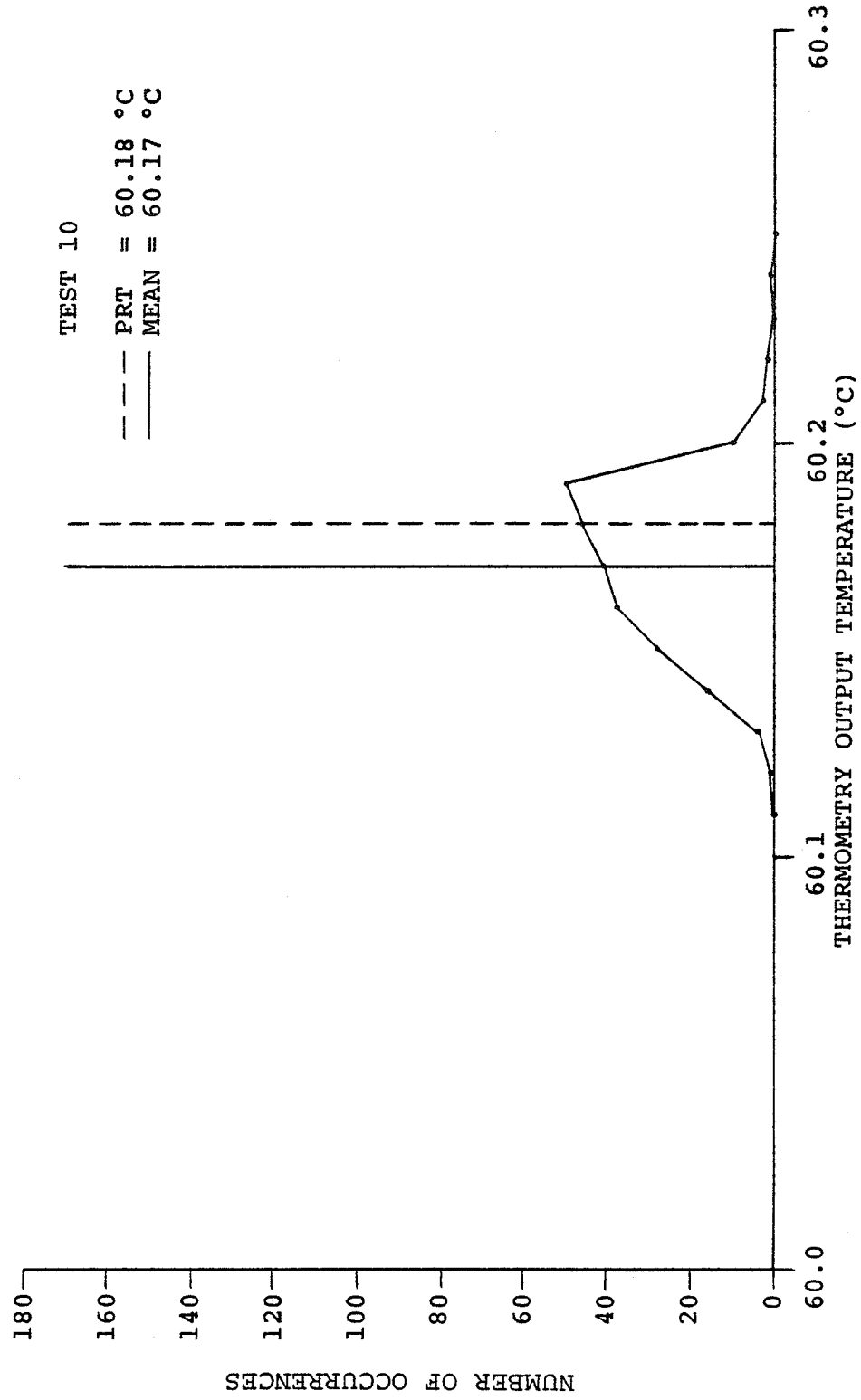


Figure 5.26. Distribution of output temperatures when probes are read every 36 seconds.

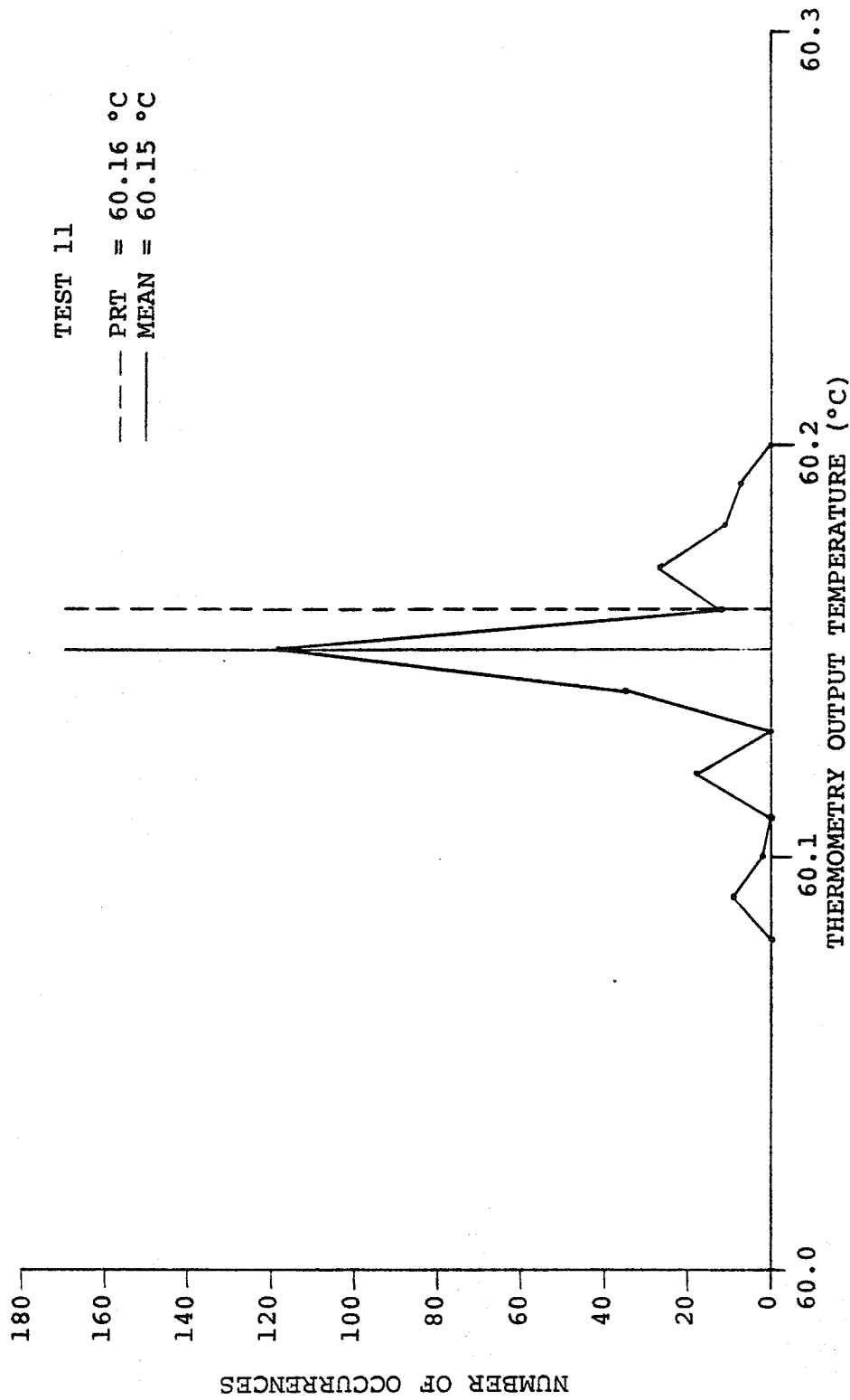


Figure 5.27. Distribution of output temperatures when probes are read every 60 seconds.

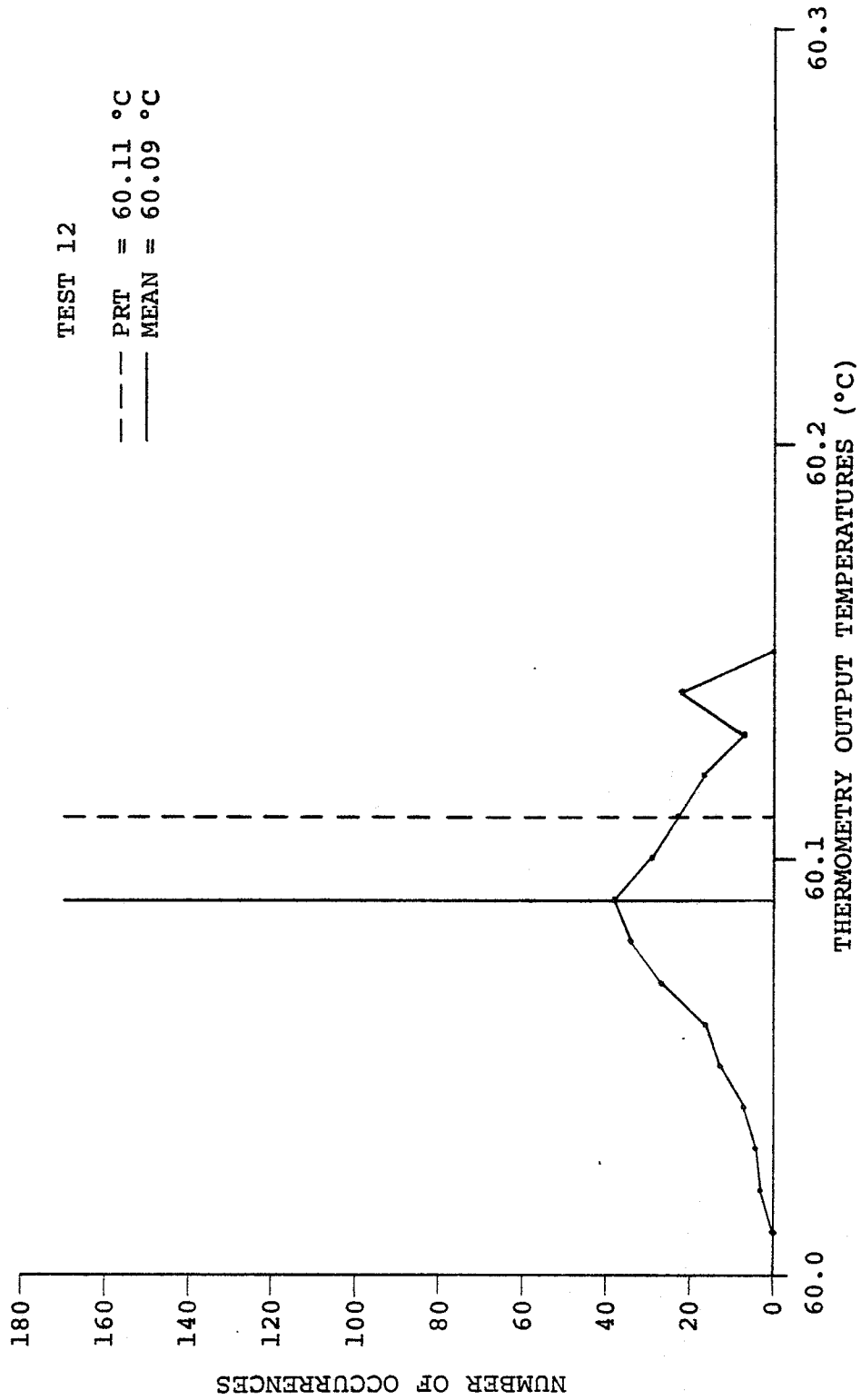


Figure 5.28. Distribution of output temperatures when probes are read every 180 seconds.

performance of the thermometry system. Figure 5.17 illustrates this point. In this plot, channels three and fifteen are responsible for all the readings below 19.85°C , causing the mean to be less than the PRT temperature. However, it is seen that the "center" of the distribution is actually above the PRT temperature. In fact, most of the points are above the PRT temperature. This means that a typical reading of output temperature will exceed the PRT temperature with a probability of greater than 50%.

Similarly, in Figures 5.21 through 5.24, channel six produced readings far above the rest of the distribution, and had the effect of pulling the mean above the PRT temperature. Channel six continued to act suspiciously in the tests illustrated in Figures 5.25 through 5.28. For each of the four tests, its output remained fixed at the second calibration temperature for the duration of the test. This peculiar behavior was masked somewhat by the fact that the second calibration point was always near the PRT temperature of about 60.14°C .

Qualitatively, one could determine the accuracy of the thermometry system, for a particular test, by how much the PRT temperature deviates from the center of the distribution. Similarly, the precision could be defined as the symmetric variation about the center of the distribution that encompasses two-thirds of the points. These definitions will de-emphasize the erratic channels and enhance the presentation of the good channels. These values of accuracy and precision are presented in Table 5.6.

Table 5.6. Rough Estimates of Accuracy and Precision from the Point Histograms.

<u>Figure</u>	<u>Accuracy (°C)</u>	<u>Precision (°C)</u>
5.17	0.01	0.02
5.18	0.01	0.03
5.19	0.00	0.01
5.20	0.01	0.01
5.21	0.00	0.02
5.22	0.00	0.04
5.23	0.02	0.03
5.24	0.00	0.03
5.25	0.01	0.00
5.26	0.01	0.02
5.27	0.01	0.01
5.28	0.02	0.03

On the whole, these values are smaller than those in Subsection 5.3.3, where no attempt was made to distinguish poor channels from good ones. However, they are very similar to the values obtained in Subsection 5.3.2, where only the five best channels were analyzed. This is as expected. Another interesting point is seen by dividing the histograms into three groups, corresponding to the PRT temperature during the tests. These groups are Figures 5.17 through 5.20, Figures 5.21 through 5.24, and Figures 5.25 through 5.28. The three groups correspond to water bath temperatures of approximately 20°C, 40°C, and 60°C, respectively. One can see that there is a definite trade-off between precision and accuracy between these groups.

5.4. Explanation of the Errors

When the calibration routine did not calibrate a particular channel properly, several possible errors might have occurred.

Small deviations in precision may be attributed to the slight temperature instability of the water bath. Small errors in accuracy may be due to errors caused by the manipulation of intermediate results in the calibration routine.

A spurious data point which was not consistent with the rest of the readings, as seen in Figure 5.9, was probably due to noise on the analog board. To eliminate such a problem, several readings of the digitized voltage from the analog-to-digital converter could be averaged. Then, this result could be used in the calculations.

When the readings were not accurate or precise, a serious problem with the probe or thermocouple amplifier chip may have existed. Another possibility is that the probe may have been

placed in the water bath improperly. The position of the thermocouple tip in relation to the PRT probe may have been such that they were actually at different temperatures when it was assumed that they were at the same temperature.

It is possible for the readings of a particular channel to be inaccurate but remain precise. The twenty-four hour run contained such an example. As can be seen in Figure 5.10, all of the readings for channel six exceed the PRT temperature of 40.10°C by greater than 0.10°C . The reason for the larger than normal deviation is probably a bad calibration. In other words, one or both of the calibration voltages obtained from the analog board were most likely in error. If the probes were placed in the exact same calibration temperature again, the voltage might have been different. If this were the case, the gain and the offset calculated would have been based on a bad input point and every output temperature would deviate greatly from the true value. As a result, all of the readings deviate by about the same amount.

One way to check for such problems would be to verify that the calibration is successful immediately after the calibration is completed. The probes could be placed in a third temperature water bath, which could be at the same temperature as the first. This temperature would be entered and the probes read. If there is a discrepancy of more than, say, 0.1°C , the particular channel would be considered to be uncalibrated. The option to recalibrate the faulty channels, without altering the correct channels, would be available. If a channel fails again, the probe or thermocouple chip is probably defective, and so the channel should not be used.

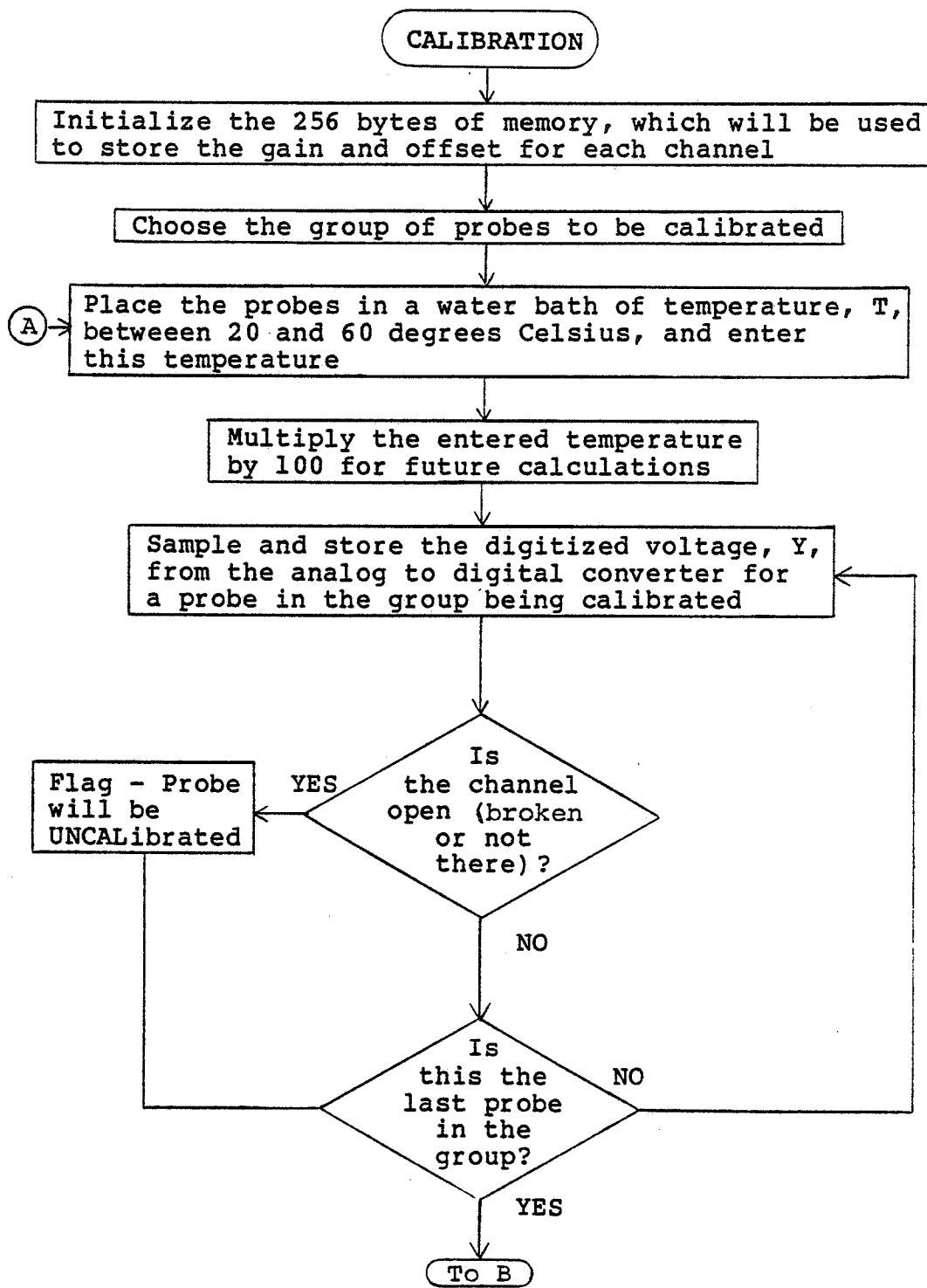
CHAPTER VI

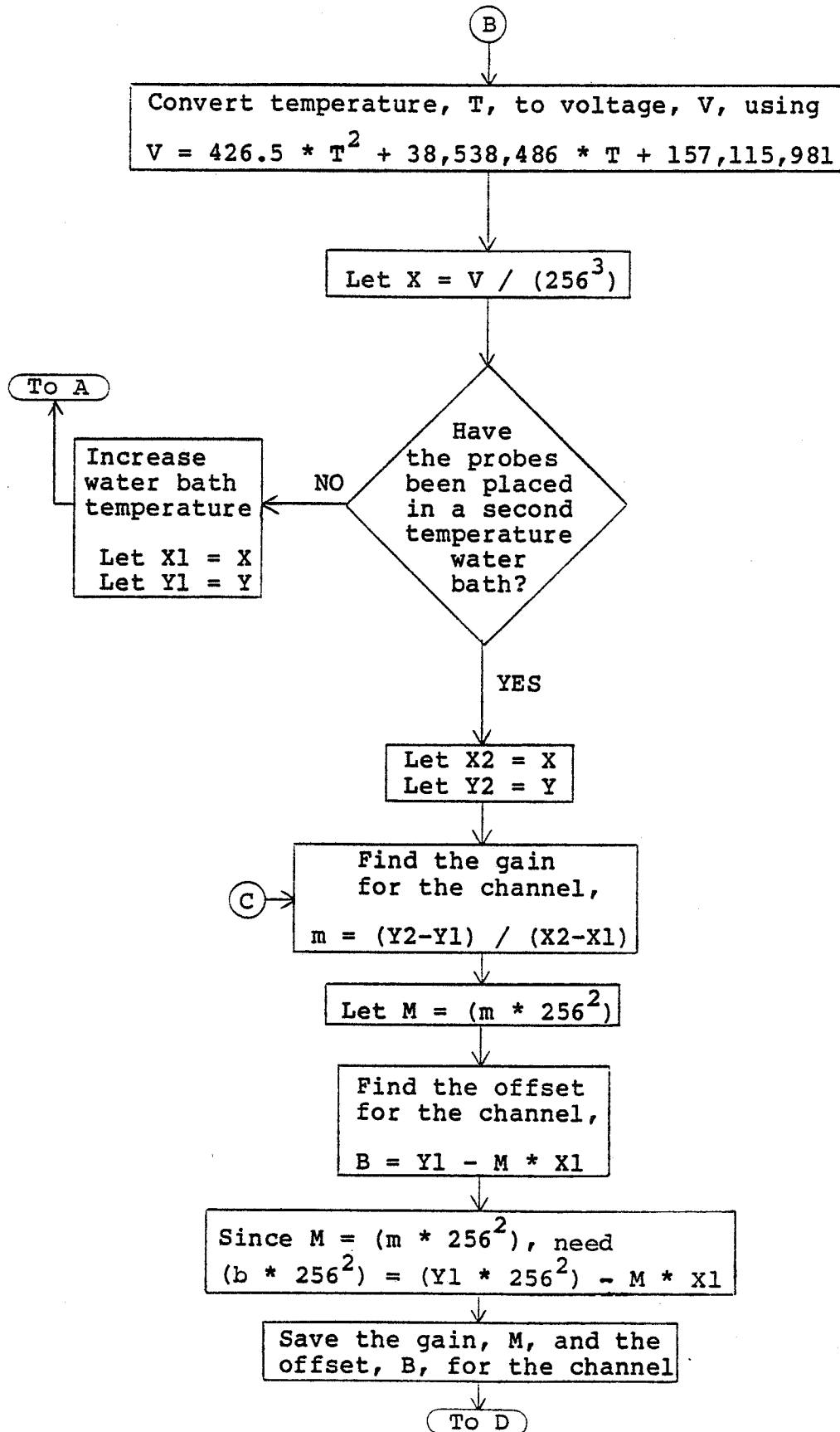
SUMMARY

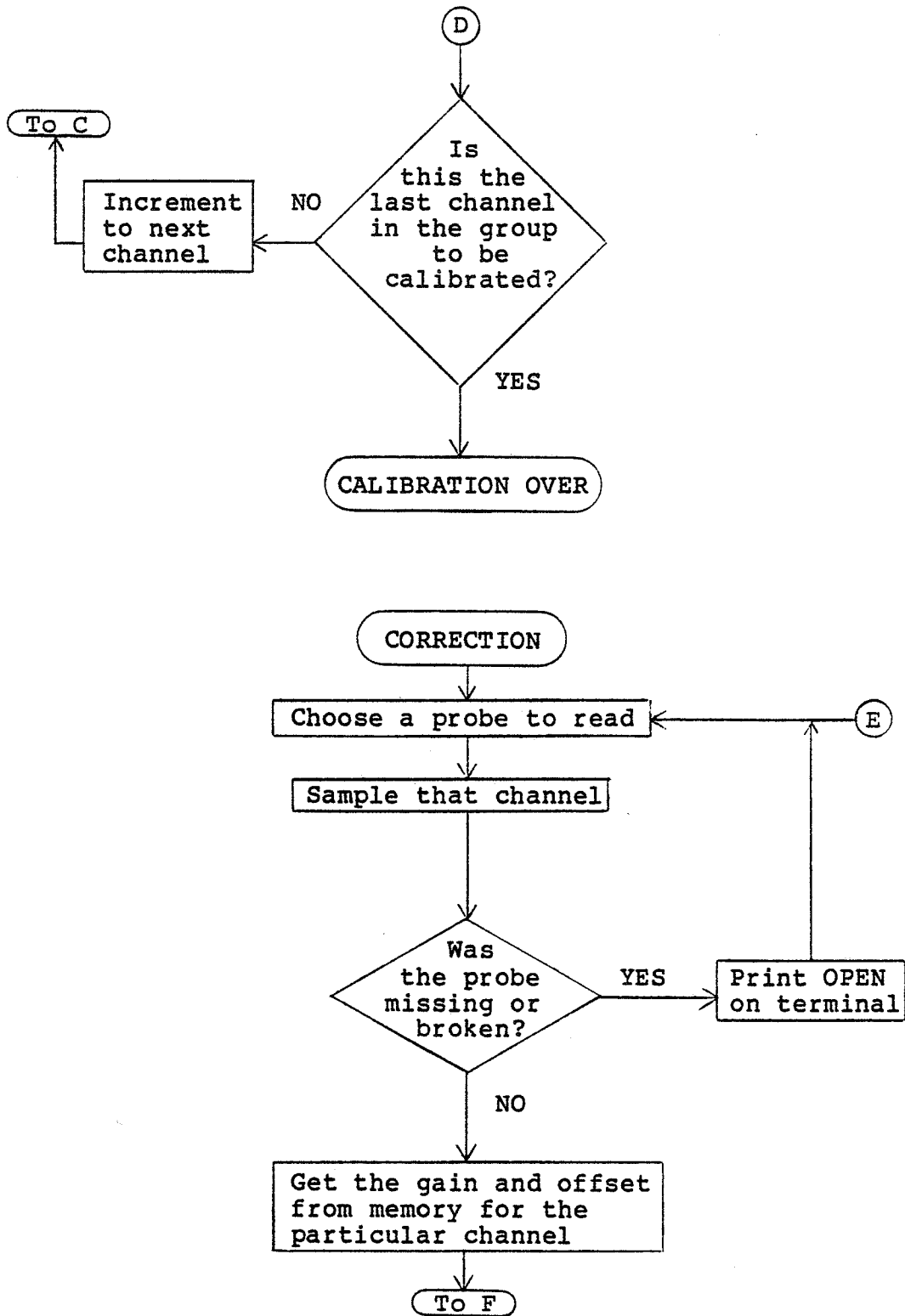
The double-point calibration routine for the thermometry system has been shown to function properly. The tests that have been performed indicate an accuracy of $\pm 0.01^{\circ}\text{C}$ and a precision of $\pm 0.03^{\circ}\text{C}$. In addition, the results are stable over long periods of time and repeatable under various conditions. Some of the reasons for unusual deviations have been discussed and a method of checking for incorrect calibrations has been suggested.

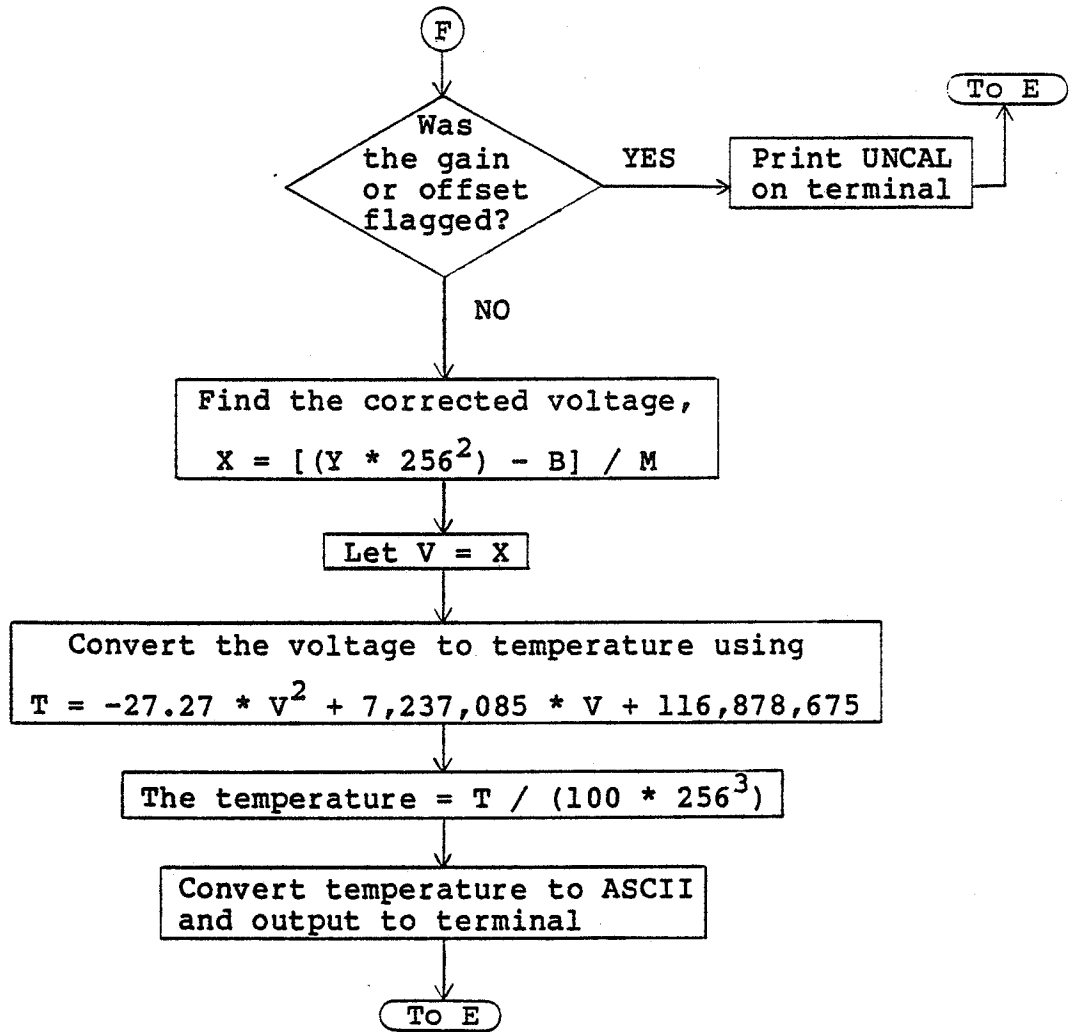
APPENDIX A

FLOW CHART FOR THE CALIBRATION ROUTINE









APPENDIX B

PROGRAM LISTING WITH CALIBRATION

```

;*****
;*          16-CHANNEL THERMOMETRY SYSYTEM          *
;*          WITH CALIBRATION                        *
;*          BY                                       *
;*          MARY OZARKA                             *
;*          UNIVERSITY OF ILLINOIS AT URBANA-CHAMPAIGN *
;*THIS PROGRAM CONTAINS ALFRED GHARAKHANI'S CONTROL CODE *
;*FOR THE THERMOMETRY SYSTEM RELATED TO INITIALIZATION, *
;*CHARACTER INPUT AND OUTPUT, AND SAMPLING OF THE A/D *
;*CONVERTER. THE CALIBRATION CODE HAS BEEN DEVELOPED FOR *
;*TYPE T THERMOCOUPLES. THE MESSAGES ARE STORED BEGINNING *
;*AT 900 HEXADECIMAL IN MEMORY. IN THE PRESENT FORM, SOME *
;*OF THE RESPONSES TO THE MESSAGES ARE NOT IN A *
;*"USER-FRIENDLY" FORM. THESE MAY BE EASILY MODIFIED. *
;*****
;
;
;
;LABELS.
0094     ALTCH     EQU P1.4
0095     START    EQU P1.5
0096     RDY      EQU P1.6
0007     BELL     EQU $07
000A     LF       EQU $0A
0020     BLANK    EQU $20
003E     PRMT     EQU $3E
000D     CR       EQU $0D
002E     POINT    EQU $2E
0087     PCON     EQU $87
F000     DATAL    EQU $F000
E000     DATAH   EQU $E000
D000     PDATAL   EQU $D000
C000     PDATAH   EQU $C000
B000     DSPLY    EQU $B000
0000     ZERD     EQU $00
000A     TEN      EQU $0A
0020     TWEN     EQU $20
0021     TWEN1    EQU $21
0040     FORT     EQU $40
0041     FORT1    EQU $41
;
;
;THIS PORTION OF THE PROGRAM CONFIGURES THE 8031 TO
;PERFORM THE DESIRED FUNCTIONS. TO UNDERSTAND THE DETAILS
;REFER TO MCS-51 USERS MANUAL (CHAP. 2). TO SIMPLIFY THIS
;PAGE NUMBERS ARE INCLUDED.

```

SOURCE FILE NAME: CAL2.ASM

```

;
0100      INIT:   ORG #100      ;START LOADING THE PROGRAM FROM
;100H.
0100 74FF      MOV A,#FF      ;TURN OFF THE 7 SEGMENTS
0102 90B000    MOV DPTR,#DSPLY
0105 F0        MOVX @DPTR,A
; IN THE NEXT THREE LINES PORT1 WILL BE CONFIGURED. RDY (P1.6)
; IS SET TO BE AN INPUT. ALTC(P1.4) IS SET AND START(P1.5)
; IS CLEARED
; CHANNEL SELECT BITS ARE ALL CLEARED. PORT3 IS CONFIGURED
; FOR ALTERNATE FUNCTIONS (REFER TO PP.13-15).
0106 759050    MOV P1,#%01010000    ;MAKE RDY AN INPUT.
0109 43B0FF    ORL P3,#%11111111
; IN THE END INTERRUPT SYSTEM IS SET UP
;
;   MOV IE,#%10000001    ;ENABLE INTO ONLY.
;   MOV IP,#%00000001    ;INTO HAS HIGHEST PRIORITY.
; FOR MORE INFO. ABOUT INTERRUPTS REFFER TO PP. 6-10
;
;
010C 1202A8    CALL BAUD      ;SET UP THE SERIAL PORT.
010F 7407      MOV A,#BELL
0111 1202FB    CALL DUTCH    ;BEEP THE TERMINAL
0114 9009E5    MOV DPTR,#%09E5
0117 120323    CALL MESS     ;PRINT "URI TERM-X"
011A 12031C    CALL PROMT   ;PROMT THE USER.
;
;
; THE MAIN ROUTINE CALIBRATES THE SET OF PROBES REQUESTED.
; THEN THE CALIBRATED TEMPERATURE OF A REQUESTED PROBE IS
; DISPLAYED.
;
011D      MAIN   EQU $
; INITIALLY LOAD THE 256 EXTERNAL MEMORY LOCATION USED TO
; STORE GAIN AND OFFSET WITH #%99
011D 120177    CALL NN
0120 1201B5    CALL PROBE   ;GET THE CHANNELS TO BE CALIBRATED
0123 120336    CALL CALIB   ;CALIBRATE THESE PROBES
0126 757000    MOV #70,#ZERO
0129 12023C    MORE:   CALL CHNL   ;SELECT A CHANNEL TO OBSERVE
012C 8F71      MOV #71,R7    ;FOR USE LATER
012E EF        SAM:   MOV A,R7
012F 120275    CALL SAMPLE  ;SAMPLE IT
; CHECK IF PROBE MISSING WHEN SAMPLED
0132 E9        MOV A,R1
0133 B4990C    CJNE A,#%99,CHX
0136 EA        MOV A,R2
0137 B49908    CJNE A,#%99,CHX
; PRINT 0
013A 744F      MOV A,#%4F
013C 1202FB    CALL DUTCH
013F 020160    JMP MORO     ;TRY AGAIN WITH WHICH PROBE?

```

SOURCE FILE NAME: CAL2.ASM

```

;
0142 120711 CHX:  CALL CORR    ;CORRECTION BASED ON OFFSET AND GAIN
;CHECK IF THE CHANNEL IS UNCALIBRATED
0145 E57C      MOV A,#7C
0147 B4990D    CJNE A,#$99,FN1
014A E57D      MOV A,#7D
014C B49908    CJNE A,#$99,FN1
;PRINT U
014F 7455      MOV A,#$55
0151 1202F8    CALL OUTCH
0154 020160    JMP MORO
;
0157 12077A    FN1:  CALL TEMP    ;CONVERT THE VOLTAGE TO TEMPERATURE
;
015A 1207D7    CALL CONV    ;CONVERT TO ASCII
015D 120826    CALL OUT     ;DISPLAY TEMPERATURE TO TERMINAL
0160 E570      MORO:  MOV A,#70
0162 B40005    CJNE A,#ZERO,MOR1
0165 12030A    CALL CRLF
0168 80BF      JMP MORE
016A 7420      MOR1:  MOV A,#$20
016C 1202F8    CALL OUTCH
016F 0571      INC $71
0171 AF71      MOV R7,$71
0173 1570      DEC $70
0175 80B7      JMP SAM
;
;WHEN COMMUNICATION WITH A HOST COMPUTER IS IMPLANTED,
;THE IDEA WILL BE TO KEEP SAMPLING ALL 32 (16) PROBES AND
;STORE THE TEMPERATURES IN A BUFFER.
;
;
;THE NN ROUTINE LOADS THE EXTERNAL MEMORY LOCATION 0 THROUGH
;255 WITH #$99
;
0177          NN      EQU $
0177 900000    MOV DPTR,#$0000
017A 7499      NN1:   MOV A,$99
017C F0        MOVX @DPTR,A
017D 0582      INC DPL
017F E582      MOV A,DPL
0181 B400F6    CJNE A,#ZERO,NN1
0184 22        RET
;
;THE PROBE ROUTINE ASKS THE USER FOR THE CHANNELS DESIRED
;(SPECIAL CODE).
;IT EXPECTS ONLY ONE CHARACTER TO BE ENTERED.
;THIS CHARACTER IS DECODED AND THE CHANNEL NUMBER OF THE
;FIRST PROBE TO BE CALIBRATED IS STORED IN LOCATION $70.
;THE CHANNEL NUMBER OF THE LAST PROBE TO BE CALIBRATED
;PLUS ONE IS STORED IN LOCATION $71.

```

SOURCE FILE NAME: CAL2.ASM

```

;PROBE IS SETUP TO WORK ON A THERMOMETRY SYSTEM WITH UP
;TO 32 CHANNELS.
;
0185      PROBE      EQU $
0185 9009BF      MOV DPTR,##09BF
0188 120323      CALL MESS
0188 120317      CALL ECHO
018E 12030A      CALL CRLF
;
0191 B46109      CJNE A,##61,PR1
0194 757000      MOV $70,#ZERO
0197 757104      MOV $71,##04
019A 02023B      JMP PRE
;
019D B46209      PR1:  CJNE A,##62,PR2
01A0 757004      MOV $70,##04
01A3 757108      MOV $71,##08
01A6 02023B      JMP PRE
;
01A9 B46309      PR2:  CJNE A,##63,PR3
01AC 757008      MOV $70,##08
01AF 75710C      MOV $71,##0C
01B2 02023B      JMP PRE
;
01B5 B46409      PR3:  CJNE A,##64,PR4
01B8 75700C      MOV $70,##0C
01BB 757110      MOV $71,##10
01BE 02023B      JMP PRE
;
01C1 B46509      PR4:  CJNE A, ##65,PR5
01C4 757000      MOV $70,#ZERO
01C7 757108      MOV $71,##08
01CA 02023B      JMP PRE
;
01CD B46609      PR5:  CJNE A,##66,PR6
01D0 757008      MOV $70,##08
01D3 757110      MOV $71,##10
01D6 02023B      JMP PRE
;
01D9 B46709      PR6:  CJNE A,##67,PR7
01DC 757000      MOV $70,#ZERO
01DF 757110      MOV $71,##10
01E2 02023B      JMP PRE
;
01E5 B46809      PR7:  CJNE A,##68,PR8
01EB 757010      MOV $70,##10
01EB 757114      MOV $71,##14
01EE 02023B      JMP PRE
;
01F1 B46909      PR8:  CJNE A,##69,PR9
01F4 757014      MOV $70,##14

```


SOURCE FILE NAME: CAL2.ASM

```

01F7 757118      MOV $71,#$18
01FA 02023B      JMP PRE
;
01FD B46A09      PR9:   CJNE A,##6A,PR10
0200 757018      MOV $70,#$18
0203 75711C      MOV $71,#$1C
0206 02023B      JMP PRE
;
0209 B46B09      PR10:  CJNE A,##6B,PR11
020C 75701C      MOV $70,#$1C
020F 757120      MOV $71,#$20
0212 02023B      JMP PRE
;
0215 B46C09      PR11:  CJNE A,##6C,PR12
0218 757010      MOV $70,#$10
021B 757118      MOV $71,#$18
021E 02023B      JMP PRE
;
0221 B46D09      PR12:  CJNE A,##6D,PR13
0224 757018      MOV $70,#$18
0227 757120      MOV $71,#$20
022A 02023B      JMP PRE
;
022D B46E09      PR13:  CJNE A,##6E,PR14
0230 757010      MOV $70,#$10
0233 757120      MOV $71,#$20
0236 02023B      JMP PRE
;
0239 2185        PR14:  JMP PROBE      ;INVALID INPUT SO TRY AGAIN
;
023B 22          PRE:   RET
;
;
;
;THE CHNL ROUTINE ASKS THE USER TO ENTER THE PROBE NUMBER
;FOR A TEMPERATURE READING.
;CHNL IS SETUP TO WORK ON A THERMOMETRY SYSTEM WITH UP TO 32
;CHANNELS.
;MAY ENTER VALUES 0 THROUGH 31 USING THE SPECIAL CODE (PAGE 52)
;THE VALUE WILL BE PUT IN R7.
;THERE IS A CHECK FOR INVALID INPUTS.
;
023C           CHNL   EQU $
023C 900950      MOV DPTR,##0950
023F 120323      CALL MESS           ;PRINT THE MESSAGE.
0242 120317      CALL ECHO
0245 F5F0       MOV B,A
0247 54F0       ANL A,##F0
0249 B43008      CJNE A,##30,FR
024C E5F0       MOV A,B
024E 540F       ANL A,##0F

```

SOURCE FILE NAME: CAL2.ASM

```

0250 FF          MOV R7,A          ;HAVE PROBE NUMBER IN R7
0251 02025D      JMP FRE
0254 B42010      FR:   CJNE A,##20,ERFR
0257 E5F0        MOV A,B
0259 C3          CLR C
025A 9410        SUBB A,##10
025C FF          MOV R7,A          ;HAVE PROBE NUMBER IN R7
025D 120300      FRE:   CALL INCH
0260 B40DD9      CJNE A,#CR,CHNL
0263 12030A      CALL CRLF
0266 22          RET

;
0267 E5F0        ERFR:  MOV A,B
0269 B44100      CJNE A,##41,CHNL
026C 757007      MOV #70,##07
026F 7F00        MOV R7,#ZERO
0271 12030A      CALL CRLF
0274 22          RET

;
;
;THE SAMPLE ROUTINE RECEIVES A CHANNEL NUMBER IN THE ACC.
;THE REQUESTED CHANNEL IS SAMPLED AND THE 12-BIT NUMBER FROM
;THE A/D IS RETURNED IN (R1,R2)
;
;ALSO, BROKEN T-COUPLES IN THE CHANNELS BEING SAMPLED
;WILL BE DETECTED AND FLAGGED, (R1,R2) = ##9999
;
0275          SAMPLE EQU #
0275 D294        SETB ALTCH
0277 5390F0      ANL P1,##F0      ;CLEAR PREVIOUS CHANNEL NUMBER
027A 4290        ORL P1,A          ;SEND OUT CHANNEL NUMBER TO AIS
027C C294        CLR ALTCH       ;LATCH THE CHANNEL NUMBER
027E D295        SETB START
0280 C295        CLR START      ;START THE A/D

;
;AT THIS POINT THE A/D WILL START ITS 25 MICROSECOND
;CONVERSION.
0282 90E000      MOV DPTR,#DATAH
0285 3096FD      JNB RDY,#        ;WAIT UNTIL THE END OF CONVERSION
0288 E0          MOVX A,@DPTR      ;LOAD ACC WITH HIGHEST 8 BITS
0289 F9          MOV R1,A
028A 90F000      MOV DPTR,#DATAL
028D E0          MOVX A,@DPTR      ;LOAD ACC WITH THE LOWER 4 BITS
028E FA          MOV R2,A
028F 30E305      JNB ACC.3,NOERR      ;CHECK FOR OPEN CHANNEL

;
0292 7999        ERR:   MOV R1,##99      ;THE SAMPLED CHANNEL IS OPEN
0294 7A99        MOV R2,##99
0296 22          RET

;
;SHIFT BITS IN (R1,R2) RIGHT 4 TIMES APPENDING ZEROS ON LEFT

```

SOURCE FILE NAME: CAL2.ASM

```

;
0297 EA      NDERR:  MOV A,R2
0298 54F0    ANL A,#F0
029A C4      SWAP A
029B FA      MOV R2,A
029C E9      MOV A,R1
029D 540F    ANL A,#0F
029F C4      SWAP A
02A0 4A      ORL A,R2
02A1 FA      MOV R2,A
02A2 E9      MOV A,R1
02A3 54F0    ANL A,#F0
02A5 C4      SWAP A
02A6 F9      MOV R1,A
;
;TST1:  MOV A,R1      ;FOR TEST
;        MOV B,R2      ;FOR TEST
;        CALL TEST3    ;FOR TEST
;
02A7 22      RET
;
;
;
;THE FOLLOWING SUBROUTINE WILL FIGURE OUT THE BAUD RATE
;SETTING. A PROPER RELOAD VALUE WILL BE LOADED ACCORDINGLY.
;IN THE END COUNTER1 WILL BE STARTED. FOR MORE INFO.
;ABOUT SERIAL PORT SET UP REFER TO PP.18-28 .
02A8 758801  BAUD:  MOV TCON,#200000001
02AB 759850    MOV SCON,#201010000
02AE 758920    MOV TMOD,#200100000
02B1 758780    MOV PCON,#80 ;DOUBLE THE BAUD RATE
02B4 90F000    MOV DPTR,#DATAL
02B7 E0        MOVX A,@DPTR ;READ THE SETTING.
02B8 5407      ANL A,#200000111
02BA B40006    CJNE A,#0,B600
02BD 758D30    MOV TH1,#30 ;300 BAUD.
02C0 0202F3    JMP GOTIT
02C3 B40106    B600:  CJNE A,#1,B1200
02C6 758D98    MOV TH1,#98 ;600 BAUD
02C9 0202F3    JMP GOTIT
02CC B40206    B1200: CJNE A,#2,B2400
02CF 758DCC    MOV TH1,#CC ;1200 BAUD.
02D2 0202F3    JMP GOTIT
02D5 B40306    B2400: CJNE A,#3,B4800
02D8 758DE6    MOV TH1,#E6 ;2400 BAUD.
02DB 0202F3    JMP GOTIT
02DE B40406    B4800: CJNE A,#4,B9600
02E1 758DF3    MOV TH1,#F3 ;4800 BAUD.
02E4 0202F3    JMP GOTIT
02E7 B40506    B9600: CJNE A,#5,B192
02EA 758DF9    MOV TH1,#F9 ;9600 BAUD.

```

SOURCE FILE NAME: CAL2.ASM

```

02ED 0202F3      JMP GOTIT
02F0 758DFD      B192:  MOV TH1,#$FD  ;19.2K BAUD.
02F3 028E       GOTIT:  SETB TR1    ;START THE TIMER.
02F5 0299       SETB TI    ;SET TI FOR 1ST CHARACTER.
02F7 22         RET
                ;
                ;OUTCH: IS A SUBROUTINE WHICH SENDS OUT THE CONTENT OF
                ;THE ACC. TO THE SERIAL BUFFER OF THE 8031,ACC. MUST
                ;CONTAIN THE 7BIT ASCII REPRESENTATION OF DESIRED
                ;CHARACTER.
                ;NOTICE THAT NO PARITY IS USED.
                ;VALUE OF ACC. REMAINS UNTOUCHED.
                ;
02FB 3099FD      OUTCH:  JNB TI,$      ;WAIT UNTIL THE END OF THE PREVIOUS
                ;TRANSMISSION.
02FB C299       CLR TI    ;GET READY FOR THE CURRENT CHAR.
02FD F599       MOV SBUF,A  ;SEND THE CURRENT CHAR.
02FF 22         RET
                ;
                ;
                ;INCH: IS A SUBROUTINE WHICH RECEIVES AN ASCII CHAR. FROM
                ;THE SERIAL BUFFER OF THE 8031. THIS CHAR. WILL BE PLACED
                ;IN THE ACC.IN THE END ACC.7 WILL BE CLEARED. PARITY IS
                ;IGNORED.
                ;
0300 3098FD      INCH:  JNB RI,$      ;WAIT FOR RECEIVE INTERRUPT
0303 C298       CLR RI    ;CLEAR THE RECEIVE INTERRUPT.
0305 E599       MOV A,SBUF
0307 547F       ANL A,#$7F
0309 22         RET
                ;
                ;
                ;CRLF: THIS IS A SUBROUTINE WHICH SENDS OUT A CR FOLLOWED
                ;BY A LF.
                ;THE VALUE IN THE ACCUM. DOES NOT CHANGE
                ;
030A F51A      CRLF:  MOV $1A,A
030C 740D       MOV A,#CR
030E 51F8       CALL OUTCH
0310 740A       MOV A,#LF
0312 51F8       CALL OUTCH
0314 E51A       MOV A,$1A
0316 22         RET
                ;
                ;
                ;ECHO: IS A SUBROUTINE WHICH RECEIVES CHAR FROM THE
                ;KEYBOARD AND SENDS IT TO THE SCREEN.ACC. WILL PRESERVE

```

SOURCE FILE NAME: CAL2.ASM

```

;THE RECEIVED CHAR.
;
;
;
0317 7100 ECHO:  CALL INCH      ;GET THE CHAR. FROM THE KEYBOARD.
0319 51FB      CALL OUTCH     ;ECHO THE CHAR TO THE SCREEN
031B 22      RET
;
;
;
;PROMT: IS A SUBROUTINE WHICH PRINTS A PROMT IN THE
;BEGINNING OF THE NEXT LINE.
;
;
;
031C 710A PROMT:  CALL CRLF
031E 743E      MOV A,#PRMT
0320 51FB      CALL OUTCH
0322 22      RET
;
;
;
;MESS: SUBROUTINE WILL PRINT DIFFERENT MESSAGES ON THE
;SCREEN. THESE MESSAGES ARE STORED IN THE PROGRAM MEMORY
;(900H-A00H). EACH MESSAGE IS IDENTIFIED BY THE ADDRESS OF
;ITS FIRST CHARACTER. THE LAST CHAR. OF EACH MESSAGE MUST
;BE A CR. THIS ROUTINE EXPECTS THE ADDRESS OF MESSAGE IN
;THE DPTR. IN THE END ACC. AND DPTR WILL BE CLEARED.
;
;
;
0323 710A MESS:  CALL CRLF
0325 7C00      MOV R4,#$00
0327 EC NEXT:   MOV A,R4      ;SAVE THE INDEX
0328 93      MOVC A,#A+DPTR
0329 B40D03    CJNE A,#CR,AGAIN ;STOP IF CR
032C 020334    JMP FINISH
032F 51FB AGAIN: CALL OUTCH   ;DISPLAY THE CHAR.
0331 0C      INC R4        ;INCREMENT THE INDEX.
0332 80F3      JMP NEXT
0334 E4 FINISH: CLR A
0335 22      RET
;
;
;
;THE CALIB ROUTINE GENERATES A CORRECTION GAIN AND OFFSET
;FOR EACH CHANNEL. THESE VALUES ARE STORED IN EXTERNAL
;NONVOLATILE RAM.
;
;THE NUMBER OF THE FIRST PROBE TO BE CALIBRATED IS PASSED
;IN LOCATION $70 AND THE LAST PROBE TO BE CALIBRATED PLUS
;ONE IS PASSED IN LOCATION $71.

```

SOURCE FILE NAME: CAL2.ASM

```

;MEMORY LOCATION $72 WILL HOLD A NUMBER COUNTER.
;
0336 CALIB EQU $
0336 900900 MOV DPTR,##0900 ;SETUP FOR FIRST MESSAGE
0339 1203A8 CALL MT
;
;MT SENDS OUT THE FIRST MESSAGE AND RETURNS THE INPUT
;TEMPERATURE, X1 IN (R4,R5)
;
033C 7820 MOV R0,#TWEN ;BEGIN STORING AT $20
033E 857072 MOV $72,$70 ;INITIALIZE $72 = FIRST CHANNEL
0341 12044E CALL LOAD
;LOAD TEMP1, Y1, 12 BIT NUMBER FROM A/D FOR ALL CHANNELS
;TO CALIBRATE.
;FIND THE VOLTAGE CORRESPONDING TO TEMPERATURE X1 IN (R4,R5)
0344 120460 CALL VOLT
;VOLT RETURNS THE VOLTAGE IN (R3,R4)
;STORE IN ($7E,$7F) SINCE VOLT IS USED AGAIN
0347 8B7E MOV $7E,R3
0349 8C7F MOV $7F,R4
;
034B 900968 MOV DPTR,##0968
034E 1203A8 CALL MT
;MT SENDS OUT THE SECOND MESSAGE AND RETURNS THE TEMPERATURE
;X2 IN (R4,R5)
0351 7840 MOV R0,#FORT ;BEGIN STORING AT $40
0353 857072 MOV $72,$70 ;INITIALIZE,$72 = FIRST CHANNEL
0356 12044E CALL LOAD
;LOAD TEMP2, Y2, 12 BIT NUMBER FROM A/D FOR ALL CHANNELS
;TO BE CALIBRATED
;FIND THE VOLTAGE CORRESPONDING TO TEMPERATURE X IN (R4,R5)
0359 120460 CALL VOLT
;
;VOLT RETURNS THE VOLTAGE IN (R3,R4).
;REMEMBER X2 > X1 SO Y2 > Y1 TOO.
;FIRST FIND (X2-X1) = (R3,R4)-($7E,$7F) AND STORE IN
;($74,$7A) BECAUSE WILL BE NEEDED FOR OTHER CHANNELS.
;
035C 03 CLR C
035D EC MOV A,R4
035E 957F SUBB A,$7F
0360 F57A MOV $7A,A
0362 EB MOV A,R3
0363 957E SUBB A,$7E ;WITH BORROW
0365 F574 MOV $74,A
;
;FIND THE GAIN = (Y2-Y1)/(X2-X1)
0367 857072 MOV $72,$70
036A 7821 MOV R0,#TWEN1
036C 7941 MOV R1,#FORT1
036E AC74 LPP: MOV R4,$74

```

SOURCE FILE NAME: CAL2.ASM

```

0370 AD7A      MOV R5,$7A
0372 1205DD    CALL GAIN
                ;THE GAIN IS RETURNED IN ($7B,$7C,$7D)
                ;FIND THE OFFSET
0375 12069C    CALL INTC
                ;OFFSET RETURNED IN ($75,$76,$77,$78,$79)
                ;STORE THE GAIN AND OFFSET IN EXTERNAL RAM
0378 1206E6    CALL SAVE
                ;SETUP FOR THE NEXT CHANNEL
037B 08        INC R0
037C 08        INC R0
037D 08        INC R0
037E 09        INC R1
037F 09        INC R1
0380 09        INC R1
                ;
0381 0572      INC $72
0383 E572      MOV A,$72
0385 B571E6    CJNE A,$71,LPP
0388 22        RET                ;END
                ;
                ;
                ;THE TEST3 ROUTINE IS FOR DEBUGGING PURPOSES ONLY.
                ;THE CONTENTS OF (A,B) ARE SENT TO THE ERROR DISPLAY ON THE
                ;FRONT OF THE THERMOMETRY SYSTEM.
0389          TEST3 EQU $
0389 F51C      MOV $1C,A
038B 85831A    MOV $1A,DPH
038E 85821B    MOV $1B,DPL
0391 90B000    MOV DPTR,#DSPLY
0394 F0        MOVX @DPTR,A
0395 7100      CALL INCH
0397 E5F0      MOV A,B
0399 90B000    MOV DPTR,#DSPLY
039C F0        MOVX @DPTR,A
039D 7100      CALL INCH
039F E51C      MOV A,$1C
03A1 851A83    MOV DPH,$1A
03A4 851B82    MOV DPL,$1B
03A7 22        RET
                ;
                ;
                ;THE MT ROUTINE SENDS OUT A MESSAGE AND RECEIVES THE
                ;TEMPERATURE VALUE IN THE FORM 23.64, FOR EXAMPLE, FOLLOWED
                ;BY A CR. THIS ROUTINE IS FOR THE STAND ALONE UNIT ONLY.
                ;THE TEMPERATURE IS MULTIPLIED BY 100 AND RETURNED IN (R4,R5)
                ;THE TEMPERATURE MUST BE IN THE RANGE BETWEEN 0 AND 99.99
                ;THERE IS NO CHECK THAT THE CHARACTERS TYPED IN ARE NUMBERS.
                ;
03AB          MT EQU $
03AB 7C00      MOV R4,#ZERO

```

SOURCE FILE NAME: CAL2.ASM

```

03AA 7D00      MOV R5,#ZERO ;CLEAR R4 AND R5
03AC 7123      REDD:  CALL MESS ;PLACE PROBES IN WATER BATH
03AE 7117      CALL ECHO ;RETURNS CHARACTER IN ACC.
03B0 B40D02    CJNE A,#CR,NT1
03B3 80F7      JMP REDD ;TRY AGAIN
;
03B5 B42E03    NT1:  CJNE A,#POINT,NT2
03B8 0203E9    JMP PT ;FIRST CHARACTER IS A DECIMAL POINT
;
03BB 540F      NT2:  ANL A,#0F ;CONVERT FROM ASCII TO HEX
03BD FD        MOV R5,A
03BE 7117      CALL ECHO ;INPUT SECOND CHARACTER
03C0 B40D03    CJNE A,#CR,NT3
03C3 020443    JMP ET100 ;MULTIPLY BY 100 TO GET VALUE
;
03C6 B42E03    NT3:  CJNE A,#POINT,NT4
03C9 0203F5    JMP PTS
;
03CC 540F      NT4:  ANL A,#0F
03CE FE        MOV R6,A
03CF ED        MOV A,R5
03D0 75F00A    MOV B,#TEN
03D3 A4        MUL AB ;B HERE SHOULD BE ZERO
03D4 C3        CLR C
03D5 2E        ADD A,R6
03D6 FD        MOV R5,A
03D7 AEF0      MOV R6,B ;LIKE CLR R6 SINCE B IS ZERO
;
03D9 7117      CALL ECHO
03DB B40D03    CJNE A,#CR,NT5
03DE 020443    JMP ET100 ;MULTIPLY BY 100 TO GET VALUE
;
03E1 B42E03    NT5:  CJNE A,#POINT,NT6
03E4 0203F5    JMP PTS
;
03E7 80C3      NT6:  JMP REDD ;TRY AGAIN
;
03E9 7117      PT:   CALL ECHO
03EB B42E02    CJNE A,#POINT,PTER
03EE 80BC      JMP REDD
03F0 B40D0F    PTER: CJNE A,#CR,ET2
03F3 80B7      JMP REDD
;
03F5 7117      PTS:  CALL ECHO
03F7 B42E02    CJNE A,#POINT,PTST
03FA 80B0      JMP REDD
03FC B40D03    PTST: CJNE A,#CR,ET2
03FF 020443    JMP ET100 ;MULTIPLY BY 100 TO GET VALUE
;
0402 540F      ET2:  ANL A,#0F
0404 FE        MOV R6,A

```


SOURCE FILE NAME: CAL2.ASM

```

0405 ED          MOV A,R5
0406 75F00A     MOV B,#TEN
0409 A4         MUL AB
040A ACFO      MOV R4,B
040C C3        CLR C
040D 2E        ADD A,R6
040E FD        MOV R5,A
                ;NOW (R4,R5) HOLD THE TEMPERATURE TO THE TENTH PLACE * 10
040F 5001      JNC ET3
0411 0C        INC R4
                ;
0412 7117     ET3:  CALL ECHO
0414 B40D12    CJNE A,#CR,NT7
                ;MULTIPLY BY TEN
0417 ED          MOV A,R5
0418 75F00A     MOV B,#TEN
041B A4         MUL AB
041C FD        MOV R5,A
041D EC        MOV A,R4
041E ACFO      MOV R4,B
0420 75F00A     MOV B,#TEN
0423 A4         MUL AB          ;B SHOULD BE ZERO
0424 2C        ADD A,R4          ;SHOULD NOT CAUSE A CARRY
0425 FC        MOV R4,A
0426 02044B    JMP ETT
                ;
0429 540F     NT7:  ANL A,#0F
042B FE        MOV R6,A
042C ED        MOV A,R5
042D 75F00A     MOV B,#TEN
0430 A4         MUL AB
0431 C3        CLR C
0432 2E        ADD A,R6
0433 FD        MOV R5,A
0434 AFF0      MOV R7,B
0436 5001      JNC NT8
0438 0F        INC R7
                ;
0439 EC        NT8:  MOV A,R4
043A 75F00A     MOV B,#TEN
043D A4         MUL AB          ;B SHOULD EQUAL ZERO
043E 2F        ADD A,R7
043F FC        MOV R4,A
0440 02044B    JMP ETT
                ;
0443 ED        ET100: MOV A,R5
0444 75F064     MOV B,#64
0447 A4         MUL AB
0448 ACFO      MOV R4,B
044A FD        MOV R5,A          ;HAVE VALUE
                ;

```

SOURCE FILE NAME: CAL2.ASM

```

044B 710A      ETT:    CALL CRLF
                ;REALLY ONLY WANT LF SINCE ALREADY HAVE CR
044D 22        RET          ;RETURNS TEMP IN (R4,R5)
                ;
                ;
                ;THE LOAD ROUTINE LOADS MEMORY LOCATIONS (BEGINNING WITH $20
                ;FOR TEMP1 AND $40 FOR TEMP2) IN BYTE PAIRS WITH THE VALUE
                ;THE A/D CONVERTER SENDS TO THE DIGITAL BOARD.
                ;
                ;R0 MUST HOLD THE BEGINNING MEMORY LOCATION.
                ;$71 HOLDS 1 PLUS THE LAST CHANNEL NUMBER.
                ;$72 HOLDS THE FIRST CHANNEL NUMBER
                ;
044E          LOAD    EQU $
044E E572      MOV A,$72      ; ACC HOLDS THE CHANNEL NUMBER
                ;
0450 5175      CALL SAMPLE
                ;SAMPLE RETURNS THE 12 BIT NUMBER FROM THE A/D CORRESPONDING
                ;TO THE CHANNEL WHOSE NUMBER WAS IN THE ACC.
                ;THE 12 BITS ARE RETURNED IN (R1,R2)
                ;IF A PROBE IS BROKEN OR NOT THERE, RETURNS (R1,R2)=$9999.
                ;
                ;STORE THIS NUMBER IN BYTE PAIRS BEGINNING AT $20, $21 FOR
                ;TEMP1 AND $40, $41 FOR TEMP2.
                ;
0452 E9        MOV A,R1
0453 F6        MOV @R0,A
0454 08        INC R0
0455 EA        MOV A,R2
0456 F6        MOV @R0,A
0457 08        INC R0
0458 0572      INC $72      ;NEXT CHANNEL
045A E572      MOV A,$72
                ;
                ;COMPARE CHANNEL NUMBER (IN $72) WITH ONE PLUS THE NUMBER OF
                ;THE LAST PROBE TO BE CALIBRATED (IN $71)
                ;
045C B571EF    CJNE A,$71,LOAD
045F 22        RET
                ;
                ;
                ;
                ;THE VOLT ROUTINE FINDS THE THERMOCOUPLE VOLTAGE BASED ON
                ;THE THERMOMETER TEMPERATURE TYPED IN AND STORED IN (R4,R5).
                ;THE EQUATION USED IS BASED ON THE TEMPERATURE-VOLTAGE
                ;STANDARD TABLES FOR T-TYPE THERMOCOUPLE PROBES
                ;THE EQUATION IS  $V = 426.5 * T^{**2} + 38,538,487 * T + 157,115,981$ 
                ;WHERE V, VOLTAGE IS IN 10**-14 VOLTS AND T, TEMPERATURE
                ;IS (100 * DEGREE C)
                ;THE VOLTAGE CALCULATED IS DIVIDED BY (256)**3 = 16,777,216
                ;AND USED IN THIS FORM WITHOUT LOSS OF ACCURACY

```

SOURCE FILE NAME: CAL2.ASM

```

;
0460      VOLT      EQU $
0460 8C7A      MOV $7A,R4
0462 9D7B      MOV $7B,R5
0464 1204BF     CALL SQU
;SQU RETURNS THE SQUARE OF (R4,R5) IN (R4,R5,R6,R7)
;THIS IS T**2
;MULTIPLY 426 * T**2
0467 7A10      MOV R2,$$10
0469 7BA9      MOV R3,$$A9      ;$$10A9 = 4265
046B 1204E7     CALL MUL24
;MUL24 MULTIPLIES (R2,R3) * (R4,R5,R6,R7)
;RESULT RETURNED IN ($75,$76,$77,$78,$79)
;DIVIDE BY TEN SINCE WANTED TO MULTIPLY BY 426.5
;INSTEAD OF 4265
046E 120595     CALL DIV51
;
;SINCE WILL NEED TO USE THE MUL24 ROUTINE AGAIN, STORE
;THE RESULT IN ($65,$66,$67,$68,$69)
;
0471 857565     MOV $65,$75
0474 857666     MOV $66,$76
0477 857767     MOV $67,$77
047A 857868     MOV $68,$78
047D 857969     MOV $69,$79
;NOW MULTIPLY 38,538,487 * T
;T WAS STORED IN ($7A,$7B)
;
0480 AA7A      MOV R2,$7A
0482 AB7B      MOV R3,$7B
0484 7C02      MOV R4,$$02
0486 7D4C      MOV R5,$$4C
0488 7E0C      MOV R6,$$0C
048A 7FF7      MOV R7,$$F7
048C 1204E7     CALL MUL24
;ADD ($75,$76,$77,$78,$79) + ($65,$66,$67,$68,$69)
;STORE VALUE IN (R3,R4,R5,R6,R7)
048F C3        CLR C
0490 E579      MOV A,$79
0492 2569      ADD A,$69
0494 FF        MOV R7,A
0495 E578      MOV A,$78
0497 3568      ADDC A,$68      ;WITH CARRY
0499 FE        MOV R6,A
049A E577      MOV A,$77
049C 3567      ADDC A,$67      ;WITH CARRY
049E FD        MOV R5,A
049F E576      MOV A,$76
04A1 3566      ADDC A,$66      ;WITH CARRY
04A3 FC        MOV R4,A
04A4 E575      MOV A,$75

```

SOURCE FILE NAME: CAL2.ASM

```

04A6 3565          ADDC A,#65      ;THERE SHOULD BE NO
04A8 FB           MOV R3,A      ;CARRY GENERATED HERE
;
;ADD 157,115,981 = 095D664DH
04A9 C3          CLR C
04AA EF          MOV A,R7
04AB 244D        ADD A,#4D
04AD FF          MOV R7,A
04AE EE          MOV A,R6
04AF 3466        ADDC A,#66      ;WITH CARRY
04B1 FE          MOV R6,A
04B2 ED          MOV A,R5
04B3 345D        ADDC A,#5D      ;WITH CARRY
04B5 FD          MOV R5,A
04B6 EC          MOV A,R4
04B7 3409        ADDC A,#09      ;WITH CARRY
04B9 FC          MOV R4,A
04BA EB          MOV A,R3
04BB 3400        ADDC A,#ZERO   ;TAKES CARE OF PREVIOUS
04BD FB           MOV R3,A      ;CARRY, IF ANY
;TRUNCATE THE LOWER THREE BYTES WHICH IS THE SAME AS
;DIVIDING BY (256)**3.
;SO THE RESULT IS IN (R3,R4).
;THIS IS DONE TO SIMPLIFY THE CODE WITHOUT LOSS OF ACCURACY
;OF THE FINAL RESULT.
;
04BE 22          RET
;
;
;THE SQU ROUTINE FINDS THE SQUARE OF THE TWO BYTE NUMBER
;STORED IN (R4,R5) AND RETURNS THE VALUE IN (R4,R5,R6,R7)
;
04BF           SQU EQU $
;FIRST MULTIPLY THE LSB TIMES ITSELF, THAT IS, (R5 * R5)
;
04BF ED          MOV A,R5
04C0 8DF0        MOV B,R5
04C2 A4          MUL AB
04C3 FF          MOV R7,A
04C4 AEFO        MOV R6,B
;
;MULTIPLY THE LSB BY THE MSB (R5 * R4) AND DOUBLE THE RESULT
;
04C6 EC          MOV A,R4
04C7 8DF0        MOV B,R5
04C9 A4          MUL AB
04CA ADF0        MOV R5,B
04CC FB          MOV R3,A      ;TEMPORARY STORAGE
04CD C3          CLR C
04CE 2B          ADD A,R3

```

SOURCE FILE NAME: CAL2.ASM

```

04CF FB          MOV R3,A
04D0 ED          MOV A,R5
04D1 3D          ADDC A,R5      ;WITH CARRY
04D2 FD          MOV R5,A
                ;ADD SHIFTED RESULT TO (R6,R7) AND GET (R5,R6,R7)
04D3 C3          CLR C
04D4 EE          MOV A,R6
04D5 2B          ADD A,R3
04D6 FE          MOV R6,A
04D7 5001        JNC SQP1
04D9 0D          INC R5
                ;
                ;MULTIPLY THE MSB BY THE MSB (R4 * R4)
                ;
04DA EC          SQP1:  MOV A,R4
04DB 8CF0        MOV B,R4
04DD A4          MUL AB
04DE ACF0        MOV R4,B
04E0 C3          CLR C
04E1 2D          ADD A,R5
04E2 FD          MOV R5,A
04E3 5001        JNC SQP2
04E5 0C          INC R4      ;RESULT IS IN (R4,R5,R6,R7)
04E6 22          SQP2:  RET
                ;
                ;
                ;
                ;THE MUL24 ROUTINE MULTIPLIES A TWO BYTE NUMBER STORED IN
                ;(R2,R3) BY A FOUR BYTE NUMBER STORED IN (R4,R5,R6,R7).
                ;THE RESULT IS RETURNED IN ($75,$76,$77,$78,$79).
                ;
04E7             MUL24 EQU $
04E7 757600      MOV $76,#ZERO
04EA 757500      MOV $75,#ZERO
04ED EF          MOV A,R7
04EE 8BF0        MOV B,R3
04F0 A4          MUL AB
04F1 85F078      MOV $78,B
04F4 F579        MOV $79,A
                ;
04F6 EF          MOV A,R7
04F7 8AF0        MOV B,R2
04F9 A4          MUL AB
04FA C3          CLR C
04FB 2578        ADD A,$78
04FD F578        MOV $78,A
04FF 85F077      MOV $77,B
0502 500A        JNC MS1
0504 E577        MOV A,$77
0506 3400        ADDC A,#ZERO  ;TAKES CARE OF CARRY IF IT EXISTS
0508 F577        MOV $77,A

```

SOURCE FILE NAME: CAL2.ASM

```

050A 5002          JNC MS1
050C 0576          INC #76

;
050E EE          MS1:  MOV A,R6
050F 8BF0          MOV B,R3
0511 A4           MUL AB
0512 C3           CLR C
0513 2578          ADD A,#78
0515 F578          MOV #78,A
0517 500A          JNC MS2
0519 E577          MOV A,#77
051B 3400          ADDC A,#ZERO ;TAKES CARE OF CARRY IF IT EXISTS
051D F577          MOV #77,A
051F 5002          JNC MS2
0521 0576          INC #76

;
0523 E5F0          MS2:  MOV A,B
0525 C3           CLR C
0526 2577          ADD A,#77
0528 F577          MOV #77,A
052A 5002          JNC MS3
052C 0576          INC #76

;
052E EE          MS3:  MOV A,R6
052F 8AF0          MOV B,R2
0531 A4           MUL AB
0532 C3           CLR C
0533 2577          ADD A,#77
0535 F577          MOV #77,A
0537 5002          JNC MS4
0539 0576          INC #76

;
053B E5F0          MS4:  MOV A,B
053D C3           CLR C
053E 2576          ADD A,#76
0540 F576          MOV #76,A
0542 5002          JNC MS5
0544 0575          INC #75

;
0546 EB          MS5:  MOV A,R3
0547 8DF0          MOV B,R5
0549 A4           MUL AB
054A C3           CLR C
054B 2577          ADD A,#77
054D F577          MOV #77,A
054F 500A          JNC MS6
0551 E576          MOV A,#76 ;INSTEAD OF INC #76
0553 3400          ADDC A,#ZERO
0555 F576          MOV #76,A
0557 5002          JNC MS6
0559 0575          INC #75

```

SOURCE FILE NAME: CAL2.ASM

```

;
055B E5F0 MS6: MOV A,B
055D C3 CLR C
055E 2576 ADD A,$76
0560 F576 MOV $76,A
0562 5002 JNC MS7
0564 0575 INC $75

;
0566 EA MS7: MOV A,R2
0567 8DF0 MOV B,R5
0569 A4 MUL AB
056A C3 CLR C
056B 2576 ADD A,$76
056D F576 MOV $76,A
056F 5002 JNC MS8
0571 0575 INC $75

;
0573 E5F0 MS8: MOV A,B
0575 2575 ADD A,$75
0577 F575 MOV $75,A ;WILL NOT HAVE CARRY HERE

;
0579 EB MOV A,R3
057A 8CF0 MOV B,R4
057C A4 MUL AB
057D C3 CLR C
057E 2576 ADD A,$76
0580 F576 MOV $76,A
0582 5002 JNC MS9
0584 0575 INC $75

;
0586 E5F0 MS9: MOV A,B
0588 2575 ADD A,$75
058A F575 MOV $75,A

;
058C EA MOV A,R2
058D 8CF0 MOV B,R4
058F A4 MUL AB ;B SHOULD EQUAL ZERO
0590 2575 ADD A,$75
0592 F575 MOV $75,A

;
0594 22 RET ;RESULT IN ($75,$76,$77,$78,$79)

;
;
00595 THE DIV51 ROUTINE DIVIDES ($75,$76,$77,$78,$79) BY (R2).
;THE RESULT IS STORED IN ($75,$76,$77,$78,$79).
;
0595 DIV51 EQU $
0595 7B00 MOV R3,$ZERO
0597 AC75 MOV R4,$75
0599 7D00 MOV R5,$ZERO
059B 1205C8 CALL SUBIT

```

SOURCE FILE NAME: CAL2.ASM

```

059E 8D75      MOV $75,R5
;
05A0 EC      MOV A,R4      ;SHIFT LEFT
05A1 FB      MOV R3,A      ;R3 SHOULD HAVE BEEN ZERO
05A2 AC76    MOV R4,$76
05A4 7D00    MOV R5,#ZERO
005A6       VALL SUBIT
05A6 8D76    MOV $76,R5
;
05A8 EC      MOV A,R4
05A9 FB      MOV R3,A
05AA AC77    MOV R4,$77
05AC 7D00    MOV R5,#ZERO
05AE 1205C8  CALL SUBIT
05B1 8D77    MOV $77,R5
;
05B3 EC      MOV A,R4
05B4 FB      MOV R3,A
05B5 AC78    MOV R4,$78
005B7       MMOV R5,#ZERO
05B7 1205C8  CALL SUBIT
05BA 8D78    MOV $78,R5
;
05BC EC      MOV A,R4
05BD FB      MOV R3,A
05BE AC79    MOV R4,$79
05C0 7D00    MOV R5,#ZERO
05C2 1205C8  CALL SUBIT
05C5 8D79    MOV $79,R5
05C7 22     RET
;
;
;THE SUBIT ROUTINE PERFORMS THE SUBTRTACTION (R3,R4) - R2
;ONLY WHEN NO CARRY (FROM R3) EXISTS.
;
05C8       SUBIT EQU $
05C8 C3     CLR C
05C9 EC     MOV A,R4
U05CA 9500  SUBB A,R2K
05CC EB     MOV A,R3
05CD 9400  SUBB A,#ZERO ;TAKE CARE OF CARRY FROM R4
05CF 5001  JNC SOSUB
05D1 22     RET
;
05D2 0D    ;SOSUB INC R5
05D3 C3    CLR C
05D4 EC    MOV A,R4
05D5 9A    SUBB A,R2
05D6 FC    MOV R4,A
05D7 EB    MOV A,R3
05D8 9400  SUBB A,#ZERO

```


AVOCET SYSTEMS 8051 CROSS-ASSEMBLER - VERSION 1.09

SOURCE FILE NAME: CAL2.ASM

```

05DA FB          MOV R3,A
05DB 80EB          JMP SUBIT      ;END OF SUBIT
;
;
;THE GAIN ROUTINE FINDS THE GAIN, M, BASED ON THE POINTS
;(X1,Y1) AND (X2,Y2)
;M = (Y2-Y1)/(X2-X1)
;(X2-X1) IS STORED IN (R4,R5) AND Y1 AND Y2 ARE STORED
;BEGINNING AT MEMORY LOCATION $20 AND $40, RESPECTIVELY,
;IN BYTE PAIRS.
;THE DIFFERENCE, (Y2-Y1) IS MULTIPLIED BY (256)**2 TO MAKE
;THE DIVISION EASIER.
;
05DD          GAIN      EQU $
;FIRST CHECK TO SEE IF THE PROBE WAS DISCONNECTED.
;THAT IS, IF Y1 OR Y2 = $$9999
;USUALLY IF ONE DOES THEY BOTH DO
05DD E6          MOV A,@R0
05DE 18          DEC R0
05DF B49908      CJNE A,$99,CH1
05E2 E6          MOV A,@R0
05E3 B49904      CJNE A,$99,CH1
;HAVE Y1 = $$9999
05E6 12061C      CALL FLAG
05E7 22          RET
;CHECK IF Y2 = $$9999
05EA E7          CH1:   MOV A,@R1
05EB 19          DEC R1
05EC B49908      CJNE A,$99,CH2
05EF E7          MOV A,@R1
05F0 B49904      CJNE A,$99,CH2
;HAVE Y2 = $$9999
05F3 12061C      CALL FLAG
05F6 22          RET
;
;NEITHER Y1 OR Y2 EQUAL $$9999 SO PROCEED WITH THE REST OF
;THE GAIN ROUTINE
05F7 08          CH2:   INC R0
05F8 09          INC R1      ;RESTORE R0 AND R1
;
05F9 C3          CLR C
05FA E7          MOV A,@R1
05FB 96          SUBB A,@R0      ;A=(LSB OF Y2)-(LSB OF Y1)
05FC FF          MOV R7,A      ;STORE LSB OF THE DIFFERENCE IN R7
;
05FD 18          DEC R0
05FE 19          DEC R1
05FF 8873        MOV $73,R0      ;SAVE R0
0601 E7          MOV A,@R1
0602 96          SUBB A,@R0      ;A = (MSB OF Y2)-(MSB OF Y1)-BORROW

```

SOURCE FILE NAME: CAL2.ASM

```

0603 FE          MOV R6,A          ;SAVE MSB OF DIFFERENCE IN R6
                ;
                ;DIVIDE (R6,R7,00,00) BY (R4,R5)
                ;(R6,R7,00,00) IS (R6,R7) * (256**2)
                ;
0604 757500     MOV $75,#ZERO
0607 8E76       MOV $76,R6
0609 8F77       MOV $77,R7
060B 757800     MOV $78,#ZERO
060E 757900     MOV $79,#ZERO
                ;
0611 7800       MOV R3,#ZERO
0613 757B00     MOV $7B,#ZERO
                ;
0616 120626     CALL DIV43
                ;THE GAIN IS RETURNED IN ($7B,$7C,$7D)
                ;THIS IS THE GAIN * (256)**2
0619 A873       MOV R0,$73        ;RESTORE R0
061B 22         RET
                ;
                ;
                ;THE FLAG ROUTINE FLAGS THE GAIN BY ASSIGNING ($7B,$7C,$7D)
                ;TO BE EQUAL TO (#$999999)
                ;
061C           FLAG EQU $
061C 757B99     MOV $7B,#$99
061F 757C99     MOV $7C,#$99
0622 757D99     MOV $7D,#$99
0625 22         RET
                ;
                ;
                ;THE DIV43 ROUTINE DIVIDES ($76,$77,$78,$79) BY (R3,R4,R5)
                ;THE METHOD USED IS LONG DIVISION
                ;THE RESULT IS STORED IN ($7B,$7C,$7D)
                ;
0626           DIV43 EQU $
                ;CHECK IF R3 = 0
0626 EB         MOV A,R3
0627 6012       JZ DD1
0629 7800       MOV R0,#ZERO
062B AF79       MOV R7,$79
062D 120663     CALL SUBOK
0630 887C       MOV $7C,R0
                ;
0632 7800       MOV R0,#ZERO
0634 7F00       MOV R7,#ZERO      ;VALUE OF R7 HERE DOES NOT MATTER
0636 120663     CALL SUBOK
0639 887D       MOV $7D,R0
                ;
063B 857778     DD1:  MOV $7B,$77
063E 857677     MOV $77,$76

```

AVOCET SYSTEMS 8051 CROSS-ASSEMBLER - VERSION 1.09

SOURCE FILE NAME: CAL2.ASM

```

0641 857576      MOV $76,$75
0644 757500      MOV $75,#ZERO
0647 7800        MOV R0,#ZERO
0649 7F00        MOV R7,#ZERO
064B 120663      CALL SUBOK
064E 887B        MOV $7B,R0

;
0650 7800        MOV R0,#ZERO
0652 7F00        MOV R7,#ZERO
0654 120663      CALL SUBOK
0657 887C        MOV $7C,R0

;
0659 7800        MOV R0,#ZERO
065B 7F00        MOV R7,#ZERO ;VALUE OF R7 HERE DOES NOT MATTER
065D 120663      CALL SUBOK
0660 887D        MOV $7D,R0

;
0662 22          RET

;
;
;
;THE SUBOK ROUTINE CHECKS IF THE SUBTRACTION OF (R3,R4,R5)
;FROM ($75,$76,$77,$78) WILL CAUSE A NEGATIVE RESULT.
;IF IT WILL, LFSH IS CALLED TO SHIFT ($76,$77,$78) ONE BYTE
;LEFT. OTHERWISE, THE SUBTRACTION IS PERFORMED UNTIL IT
;CAUSES A NEGATIVE RESULT.
;
;THE NUMBER OF SUBTRACTIONS IS RETURNED IN R0
;
0663      SUBOK   EQU $
0663 C3          CLR C
0664 E578        MOV A,$78
0666 9D          SUBB A,R5
0667 E577        MOV A,$77
0669 9C          SUBB A,R4 ;WITH BORROW
066A E576        MOV A,$76
066C 9B          SUBB A,R3 ;WITH BORROW
066D E575        MOV A,$75
066F 9400        SUBB A,#ZERO ;WITH BORROW
0671 5004        JNC QR1 ;MAY SUBTRACT
;IF THERE IS A CARRY HERE, NEED TO SHIFT ONE BYTE LEFT
0673 120690      CALL LFSH
0676 22          RET

;
0677 08          QR1: INC R0
0678 C3          CLR C ;THIS TIME STORE THE RESULT
0679 E578        MOV A,$78
067B 9D          SUBB A,R5
067C F578        MOV $7B,A
067E E577        MOV A,$77
0680 9C          SUBB A,R4 ;WITH BORROW

```

SOURCE FILE NAME: CAL2.ASM

```

0681 F577      MOV $77,A
0683 E576      MOV A,$76
0685 9B        SUBB A,R3      ;WITH BORROW
0686 F576      MOV $76,A
0688 E575      MOV A,$75
068A 9400      SUBB A,#ZERO  ;WITH BORROW
068C F575      MOV $75,A
068E 80D3      JMP SUBOK   ;END
;
;
;
;THE LFSH ROUTINE SHIFTS THE BYTES IN ($76,$77,$78,$79)
;LEFT ONE BYTE.  THE VALUE IN R7 IS SHIFTED IN ON THE RIGHT
;AND THE LEFT BYTE IS SHIFTED INTO $75.
;THE RESULT IS IN ($75,$76,$77,$78).
;
0690          LFSH   EQU $
0690 857675    MOV $75,$76
0693 857776    MOV $76,$77
0696 857877    MOV $77,$78
0699 8F78      MOV $78,R7
069B 22        RET
;
;
;
;THE INTC ROUTINE FINDS THE OFFSET B = Y1 - M * X1.
;FIRST MULTIPLY M * X1
;X1 IS STORED IN ($7E,$7F), (VOLTAGE)
;(M * 256**2) IS STORED IN ($7B,$7C,$7D)
;
069C          INTC   EQU $
;FIRST CHECK IF THE GAIN IS FLAGGED ##999999
069C E57B      MOV A,$7B
069E B4991A    CJNE A,##99,W1
06A1 E57C      MOV A,$7C
06A3 B49915    CJNE A,##99,W1
06A6 E57D      MOV A,$7D
06A8 B49910    CJNE A,##99,W1
;HAVE GAIN FLAGGED SO FLAG THE OFFSET WITH ##99 99 99 99
06AB 757599    MOV $75,##99
06AE 757699    MOV $76,##99
06B1 757799    MOV $77,##99
06B4 757899    MOV $78,##99
06B7 757999    MOV $79,##99
06BA 22        RET
;
;GAIN NOT FLAGGED SO PROCEED WITH NORMAL INTC ROUTINE
06BB AA7E      W1:   MOV R2,$7E
06BD AB7F      MOV R3,$7F
06BF 7C00      MOV R4,#ZERO
06C1 AD7B      MOV R5,$7B

```

SOURCE FILE NAME: CAL2.ASM

```

06C3 AE7C      MOV R6,$7C
06C5 AF7D      MOV R7,$7D
06C7 91E7      CALL MUL24
                ;RESULT RETURNED IN ($75,$75,$77,$78,$79)
                ;SUBTRACT Y1 - (M * X1)
06C9 08        INC R0
06CA C3        CLR C
06CB E4        CLR A
06CC 9579      SUBB A,$79
06CE F579      MOV $79,A
06D0 E4        CLR A
06D1 9578      SUBB A,$78      ;WITH BORROW
06D3 F578      MOV $78,A
06D5 E6        MOV A,@R0
06D6 9577      SUBB A,$77      ;WITH BORROW
06DB F577      MOV $77,A
06DA 18        DEC R0
06DB E6        MOV A,@R0
06DC 9576      SUBB A,$76      ;WITH BORROW
06DE F576      MOV $76,A
06E0 E4        CLR A
06E1 9575      SUBB A,$75      ;WITH BORROW
06E3 F575      MOV $75,A      ;IGNORE THE CARRY

                ;
06E5 22        RET

                ;
                ;
                ;
                ;THE SAVE ROUTINE LOADS THE GAIN AND THE OFFSET INTO
                ;EXTERNAL RAM.
                ;THE GAIN REQUIRES 3 BYTES AND THE OFFSET REQUIRES 5 BYTES
                ;SO EVERY EIGHTH BYTE BEGINS A NEW GAIN AND OFFSET FOR A
                ;DIFFERENT CHANNEL.
                ;
06E6          SAVE EQU $
06E6 E572      MOV A,$72
06EB 75F008     MOV B,$#08
06EB A4        MUL AB      ;B IS ZERO HERE
06EC 758300     MOV DPH,#ZERO
06EF F582      MOV DPL,A
06F1 E57B      MOV A,$7B
06F3 F0        MOVX @DPTR,A
06F4 A3        INC DPTR
06F5 E57C      MOV A,$7C
06F7 F0        MOVX @DPTR,A
06FB A3        INC DPTR
06F9 E57D      MOV A,$7D
06FB F0        MOVX @DPTR,A      ;HAVE GAINED STORED
06FC A3        INC DPTR
06FD E575      MOV A,$75
06FF F0        MOVX @DPTR,A

```

SOURCE FILE NAME: CAL2.ASM

```

0700 A3          INC DPTR
0701 E576       MOV A,$76
0703 F0        MOVX @DPTR,A
0704 A3        INC DPTR
0705 E577       MOV A,$77
0707 F0        MOVX @DPTR,A
0708 A3        INC DPTR
0709 E578       MOV A,$78
070B F0        MOVX @DPTR,A
070C A3        INC DPTR
070D E579       MOV A,$79
070F F0        MOVX @DPTR,A ;HAVE OFFSET STORED
0710 22        RET

;
;
;
;THE CORR ROUTINE FINDS THE CORRECTED TEMPERATURE USING THE
;STORED GAIN AND OFFSET FOR THE PARTICULAR CHANNEL.
;IT IS CALLED WITH (R1,R2) = Y, THE 12 BIT NUMBER READ FROM
;THE A/D AND R7 HOLDING THE CHANNEL NUMBER.
;
;FINDS X IN Y = M * X + B
;THAT IS X = (Y - B) / M
;
0711          CORR EQU $
0711 120750     CALL REC

;
;REC RETURNS THE GAIN IN ($7B,$7C,$7D) AND THE OFFSET IN
;($75,$76,$77,$78,$79) FOR THE CHANNEL WHOSE NUMBER IS IN R7
;
;CHECK IF THE GAIN IS FLAGGED WHICH IMPLIES THAT THE OFFSET
;IS ALSO, SO NO NEED TO CHECK BOTH.
0714 E57B       MOV A,$7B
0716 B49911     CJNE A,$99,Q1
0719 E57C       MOV A,$7C
071B B4990C     CJNE A,$99,Q1
071E E57D       MOV A,$7D
0720 B49907     CJNE A,$99,Q1
;THE GAIN IS FLAGGED SO FLAG X IN ($7C,$7D)
0723 757C99     MOV $7C,$99
0726 757D99     MOV $7D,$99
0729 22        RET

;
;SUBTRACT (Y-B), THAT IS ACTUALLY ((Y*(256**2) - B)
;
072A C3        Q1: CLR C
072B 7400       MOV A,$ZERO
072D 9579       SUBB A,$79
072F F579       MOV $79,A
0731 7400       MOV A,$ZERO
0733 957B       SUBB A,$7B ;WITH BORROW

```

SOURCE FILE NAME: CAL2.ASM

```

0735 F578      MOV $78,A
0737 EA        MOV A,R2
0738 9577      SUBB A,$77      ;WITH BORROW
073A F577      MOV $77,A
073C E9        MOV A,R1
073D 9576      SUBB A,$76      ;WITH BORROW
073F F576      MOV $76,A
0741 7400      MOV A,#ZERO
0743 9575      SUBB A,$75      ;WITH BORROW
0745 F575      MOV $75,A      ;$75 HERE SHOULD BE 0
;
;($75,$76,$77,$78,$79) = (Y - B)
;DIVIDE (Y - B) / M = X
;
0747 AB7B      MOV R3,$7B
0749 AC7C      MOV R4,$7C
074B AD7D      MOV R5,$7D
;
074D D126      CALL DIV43      ;RETURNS X IN ($7B,$7C,$7D)
;
074F 22        RET
;
;
;
;THE REC ROUTINE LOADS THE GAIN AND OFFSET FROM RAM, FOR THE
;CHANNEL NUMBER STORED IN R7, INTO MEMORY LOCATIONS
;($7B,$7C,$7D) AND ($75,$76,$77,$78,$79) RESPECTIVELY.
;
0750          REC      EQU $
;FIND THE BEGINNING ADDRESS FOR THE PARTICULAR CHANNEL
0750 EF        MOV A,R7
0751 75F008    MOV B,#08
0754 A4        MUL AB      ;B IS ZERO
0755 758300    MOV DPH,#ZERO
0758 F582      MOV DPL,A
;
075A E0        MOVX A,@DPTR
075B F57B      MOV $7B,A
075D A3        INC DPTR
075E E0        MOVX A,@DPTR
075F F57C      MOV $7C,A
0761 A3        INC DPTR
0762 E0        MOVX A,@DPTR
0763 F57D      MOV $7D,A      ;HAVE GAIN IN ($7B,$7C,$7D)
;
0765 A3        INC DPTR
0766 E0        MOVX A,@DPTR
0767 F575      MOV $75,A
0769 A3        INC DPTR
076A E0        MOVX A,@DPTR
076B F576      MOV $76,A

```

SOURCE FILE NAME: CAL2.ASM

```

076D A3          INC DPTR
076E E0          MOVX A,@DPTR
076F F577        MOV $77,A
0771 A3          INC DPTR
0772 E0          MOVX A,@DPTR
0773 F578        MOV $78,A
0775 A3          INC DPTR
0776 E0          MOVX A,@DPTR
0777 F579        MOV $79,A      ;HAVE OFFSET IN ($75,$76,$77,$78,$79)
;
0779 22          RET
;
;
;
;THE TEMP ROUTINE FINDS THE TEMPERATURE BASED ON THE VOLTAGE
;STORED IN ($7C,$7D). THE EQUATION USED IS
;T = -27.27 * V**2 + 7,237,085 * V + 116,878,675
;WHEN THE RESULTING T IS DIVIDED BY (256**3), HAVE THE
;TEMPERATURE * 100 WHICH IS STORED IN (R0,R1).
;
077A          TEMP EQU $
077A AC7C        MOV R4,$7C
077C AD7D        MOV R5,$7D
077E 91BF        CALL SQU
;SQU RETURNS THE SQUARE OF (R4,R5) IN (R4,R5,R6,R7)
;MULTIPLY 2727 * (V**2)
0780 7A0A        MOV R2,$#0A
0782 7BA7        MOV R3,$#A7
0784 91E7        CALL MUL24
;MUL24 MULTIPLIES (R2,R3) * (R4,R5,R6,R7)
;RESULT RETURNED IN ($75,$76,$77,$78,$79)
;NEXT DIVIDE BY 100 SINCE REALLY WANTED 27.27 INSTEAD OF
;2727 MULTIPLIED BY V**2.
0786 7A64        MOV R2,$#64
0788 B195        CALL DIV51
;SINCE NEED TO USE MUL24 ROUTINE AGAIN, STORE THE RESULT IN
;($65,$66,$67,$68,$69).
;
078A 857565      MOV $65,$75
078D 857666      MOV $66,$76
0790 857767      MOV $67,$77
0793 857868      MOV $68,$78
0796 857969      MOV $69,$79
;NOW MULTIPLY 7,237,085 * V
;V WAS STORED IN ($7C,$7D)
;
0799 AA7C        MOV R2,$7C
079B AB7D        MOV R3,$7D
079D 7C00        MOV R4,#ZERO
079F 7D6E        MOV R5,$#6E
07A1 7E6D        MOV R6,$#6D

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SOURCE FILE NAME: CAL2.ASM

```

07D7      CONV      EQU $
           ;DIVIDE (R0,R1) BY 10.  THE REMAINDER IS THE LEAST
           ;SIGNIFICANT DIGIT OF THE ASCII EQUIVALENT
07D7 7A00      MOV R2,#ZERO
07D9 7B00      MOV R3,#ZERO
07DB 1207FF    CALL DIV21
           ;RETURNS THE QUOTIENT IN (R2,R3) AND THE REMAINDER IN R1
07DE E9       MOV A,R1
07DF 4430     ORL A,##30      ;TO CONVERT TO ASCII
07E1 FF       MOV R7,A
           ;
           ;REPEAT THE DIVISION TWO MORE TIMES TO GET THE NEXT 2 BYTES
           ;SETUP FOR DIV21
07E2 EA       MOV A,R2
07E3 FB       MOV R0,A
07E4 EB       MOV A,R3
07E5 F9       MOV R1,A
07E6 7A00     MOV R2,#ZERO
07EB 7B00     MOV R3,#ZERO
07EA 1207FF   CALL DIV21      ;QUOTIENT IN (R2,R3), BUT R2=00
           ;
07ED E9       MOV A,R1
07EE 4430     ORL A,##30
07F0 FE       MOV R6,A
           ;
07F1 EB       MOV A,R3
07F2 75F00A   MOV B,#TEN
07F5 B4       DIV AB
           ;THE REMAINDER B IS THE THIRD BYTE
           ;A HOLDS THE FOURTH BYTE
07F6 4430     ORL A,##30
07F8 FC       MOV R4,A
           ;
07F9 E5F0     MOV A,B
07FB 4430     ORL A,##30
07FD FD       MOV R5,A
           ;
07FE 22       RET
           ;
           ;
           ;THE DIV21 ROUTINE DIVIDES THE TWO BYTE NUMBER IN (R0,R1).
           ;BY 10 USING LONG DIVISION
           ;STORE THE RESULT IN (R2,R3) AND THE REMAINDER IN R1.
           ;
07FF      DIV21   EQU $
           ;CHECK IF THE SUBTRACTION CAUSED A BORROW
07FF C3       CLR C
0800 E8       MOV A,R0
0801 940A     SUBB A,#TEN
0803 5003     JNC RR1
0805 020810   JMP RR2

```

SOURCE FILE NAME: CAL2.ASM

```

;
0808 0A   RR1:   INC R2
0809 C3           CLR C
080A EB           MOV A,R0
080B 940A        SUBB A,#TEN
080D FB           MOV R0,A   ;STORE THIS TIME
080E 80EF        JMP DIV21

;
0810 C3   RR2:   CLR C
0811 E9           MOV A,R1
0812 940A        SUBB A,#TEN
0814 EB           MOV A,R0
0815 9400        SUBB A,#ZERO ;WITH BORROW
0817 5001        JNC RR3
0819 22           RET

;QUOTIENT RETURNED IN (R2,R3) AND REMAINDER IN R1
;
081A 0B   RR3:   INC R3
081B C3           CLR C
081C E9           MOV A,R1
081D 940A        SUBB A,#TEN
081F F9           MOV R1,A
0820 EB           MOV A,R0
0821 9400        SUBB A,#ZERO ;WITH BORROW
0823 FB           MOV R0,A
0824 80EA        JMP RR2   ;END OF DIV21

;
;
;THE OUT ROUTINE WILL OUTPUT THE TEMPERATURE STORED IN
;(R4,R5,R6,R7) IN ASCII BYTES TO THE TERMINAL.
;
0826           OUT   EQU $
0826 EC           MOV A,R4
0827 1202F8       CALL OUTCH
082A ED           MOV A,R5
082B 1202F8       CALL OUTCH
082E 742E         MOV A,#POINT
0830 1202F8       CALL OUTCH
0833 EE           MOV A,R6
0834 1202F8       CALL OUTCH
0837 EF           MOV A,R7
0838 1202F8       CALL OUTCH
083B 22           RET

;
0000           END

```

SOURCE FILE NAME: CAL2.ASM

---- SYMBOL TABLE ----

ACC	00E0	DSPLY	9000	MS2	0523	PR1	019D	RR3	081A
AGAIN	032F	ECHO	0317	MS3	052E	PR10	0209	SAM	012E
ALTCH	0094	ERFR	0267	MS4	053B	PR11	0215	SAMPLE	0275
B	00F0	ERR	0292	MS5	0546	PR12	0221	SAVE	06E6
B1200	02CC	ET100	0443	MS6	055B	PR13	022D	SBUF	0099
B192	02F0	ET2	0402	MS7	0566	PR14	0239	SCON	0098
B2400	02D5	ET3	0412	MS8	0573	PR2	01A9	SOSUB	05D2
B4800	02DE	ETT	0448	MS9	0586	PR3	01B5	SGP1	04DA
B600	02C3	FINISH	0334	NT	03A8	PR4	01C1	SGP2	04E6
B9600	02E7	FLAG	061C	MUL24	04E7	PR5	01CD	SQU	04BF
BAUD	02A8	FN1	0157	NEXT	0327	PR6	01D9	START	0095
BELL	0007	FORT	0040	NN	0177	PR7	01E5	SUBIT	05C8
BLANK	0020	FORT1	0041	NN1	017A	PR8	01F1	SUBOK	0663
CALIB	0336	FR	0254	NOERR	0297	PR9	01FD	TCON	0088
CHI	05EA	FRE	025D	NT1	03B5	PRE	023B	TEMP	077A
CH2	05F7	GAIN	05DD	NT2	03BB	PRMT	003E	TEN	000A
CHNL	023C	GDTIT	02F3	NT3	03C6	PROBE	01B5	TEST3	03B9
CHX	0142	INCH	0300	NT4	03CC	PROMT	031C	TH1	008D
CONV	07D7	INIT	0000	NT5	03E1	PT	03E9	THE	0595
CORR	0711	INTC	069C	NT6	03E7	PTER	03F0	TI	0099
CR	000D	LF	000A	NT7	0429	PTS	03F5	TMOD	0089
CRLF	030A	LFSH	0690	NT8	0439	PTST	03FC	TR1	008E
DATAH	E000	LOAD	044E	OUT	0826	Q1	072A	TWEN	0020
DATAL	F000	LPP	036E	OUTCH	02FB	QR1	0677	TWEN1	0021
DD1	063B	MAIN	011D	P1	0090	RDY	0096	VOLT	0460
DIV21	07FF	MESS	0323	P3	0080	REC	0750	W1	06BB
DIV43	0626	MORO	0160	PCON	0087	REDD	03AC	ZERO	0000
DIV51	0595	MOR1	016A	PDATAH	C000	RI	0098		
DPH	0083	MORE	0129	PDATAL	D000	RR1	0808		
DPL	0082	MS1	050E	POINT	002E	RR2	0810		

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